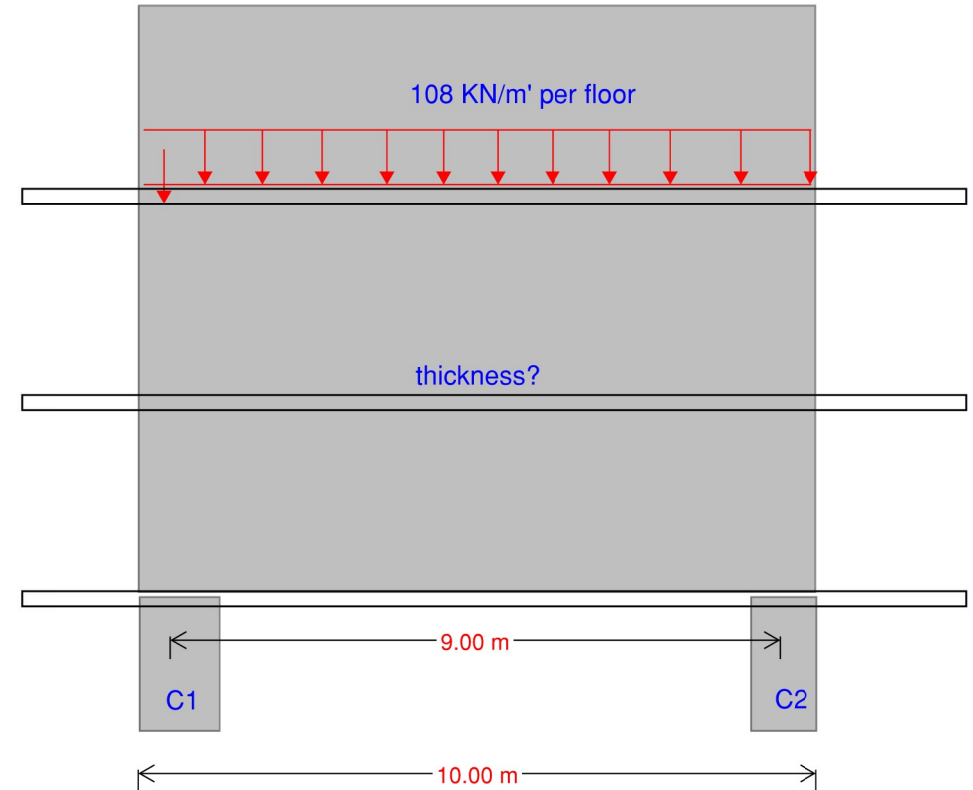
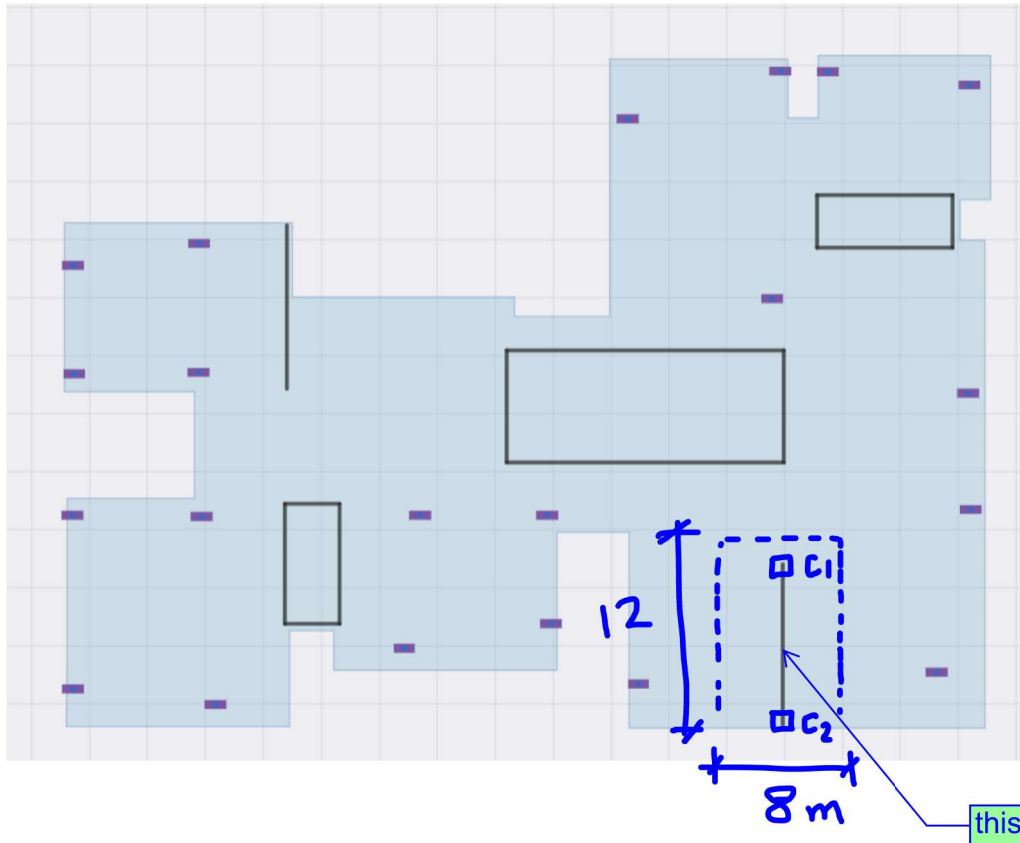




Sample Structure

Wall is supporting 20 storey building and has a tributary width (into page) of 8 meters, see plan below.

Wall thickness is decided at upper levels from building lateral scheme to achieve target period and sway, however, thickness at lower levels needs to be confirmed at transfer level. and wall to be designed to AS3600-2018



Elevation of the Wall





Gravity Loads

A - Dead Loads

- 1 - Typical slab thickness = 220 (5.5 KPa)
- 2 - Finishes (residential) = 1.5 KPa
- 3- Own weight of wall = $0.25 \times 3 \times 25 \times 10 = 187.5$ KN per level

SEE
AS1170.1

B- Live Loads

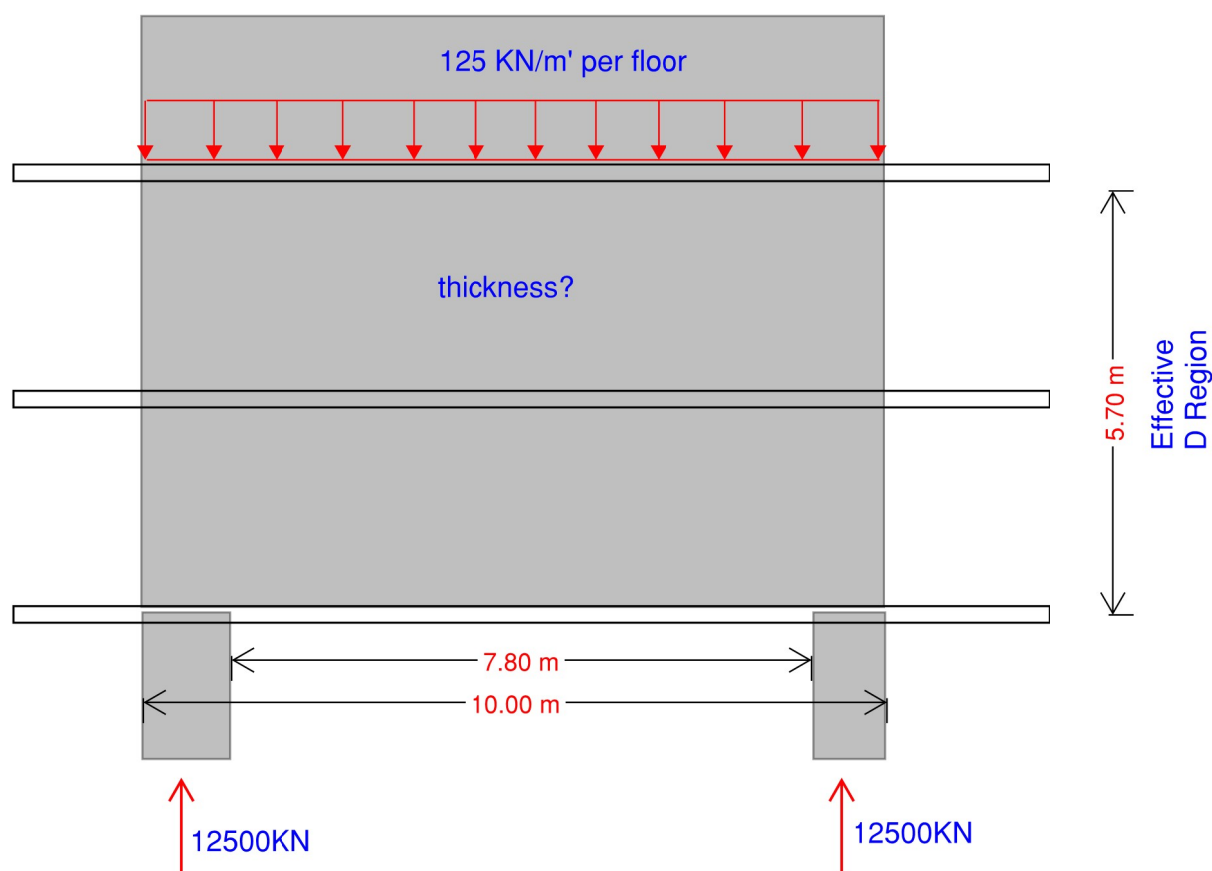
- 1 - Live loads (residential) = 1.5 KPa

Total line load on wall (Ultimate)

- 1- Slabs = $[1.2 \times (5.5 + 1.5) + 1.5 \times 1.5] \times (8 \times 12) \times 20 \text{ Levels} / 10 = 2045$ KN/m'
- 2- Wall self weight = $1.2 \times (187.5 \times 20) / 10 = 450$ KN/m'

therefore total line load = 2495 , say 2500 KN/m' ULS (or 125KN/m' per level)

total load onto wall = 25 000 KN



NOTES

Lateral loads are not likely to govern the design, ignored in this demonstration for simplicity, will assume loading is uniform over the entire width of the wall, noting the northern column C1 takes more load for the bigger tributary area



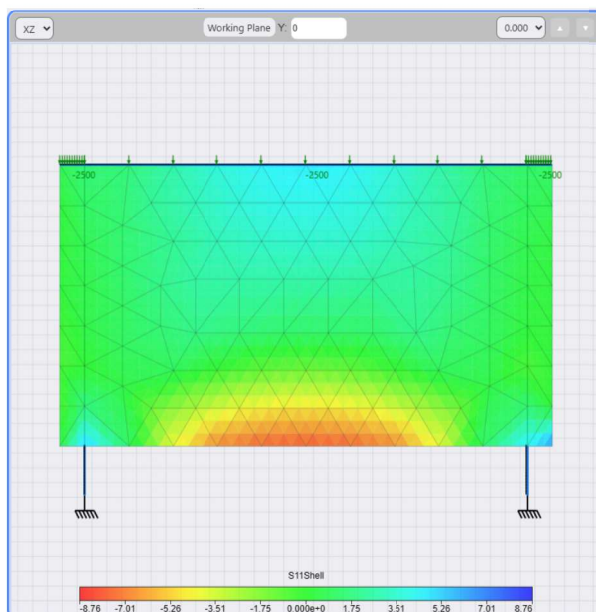
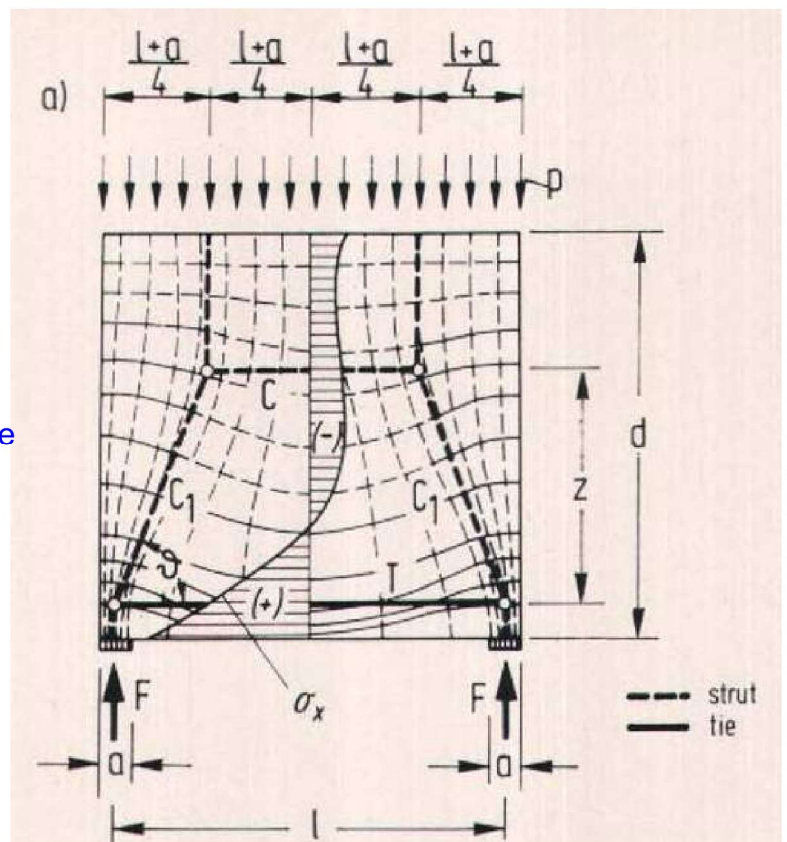
Theory

Shear walls landing on columns experience uniform stresses until the D-Region, which is the vertical distance above the supports, roughly estimated at 0.8 of the clear span.

With concrete, elastic stress distribution will not hold correct past cracking capacity of concrete. (modulus of rupture at direct tension or at stress of 1 MPa to be conservative).

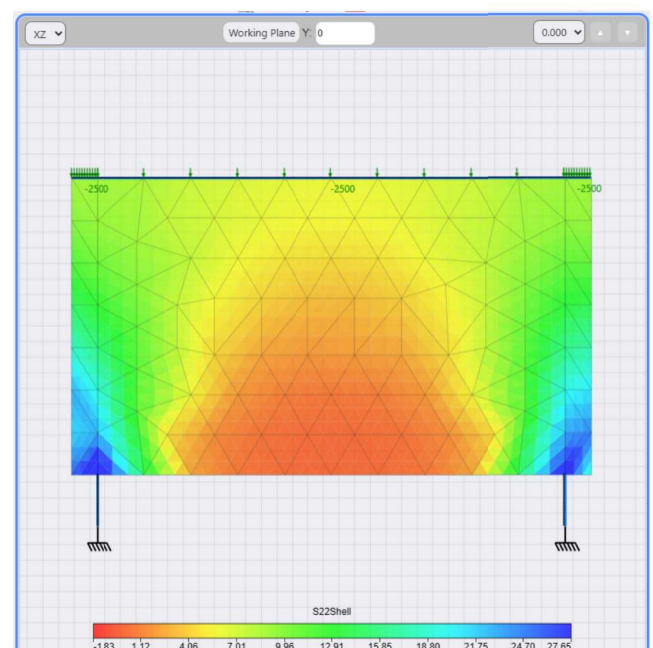
This will require rebar to be designed as area and anchorage to take the forces.

Wall bearing points must also survive compression stresses



See elastic stresses distribution
(FEAKalc 3D analysis - S11 horizontal)

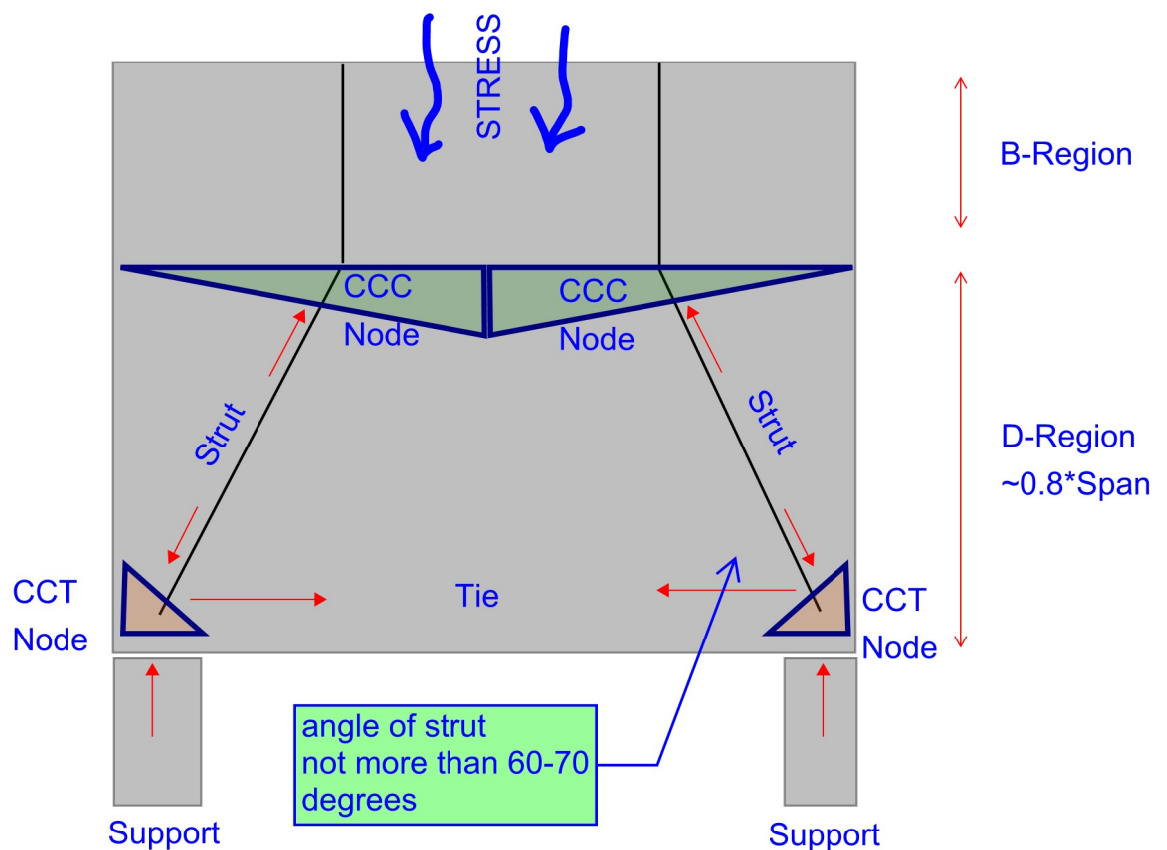
See elastic stresses distribution
(FEAKalc 3D analysis - S22 vertical)





Theory

Below is idealisation of strut and tie model, which is lower bound that takes all of the load in tension through rebar



Codes of practice provided guide on how to pass stresses through concrete, depending on element taking the load:

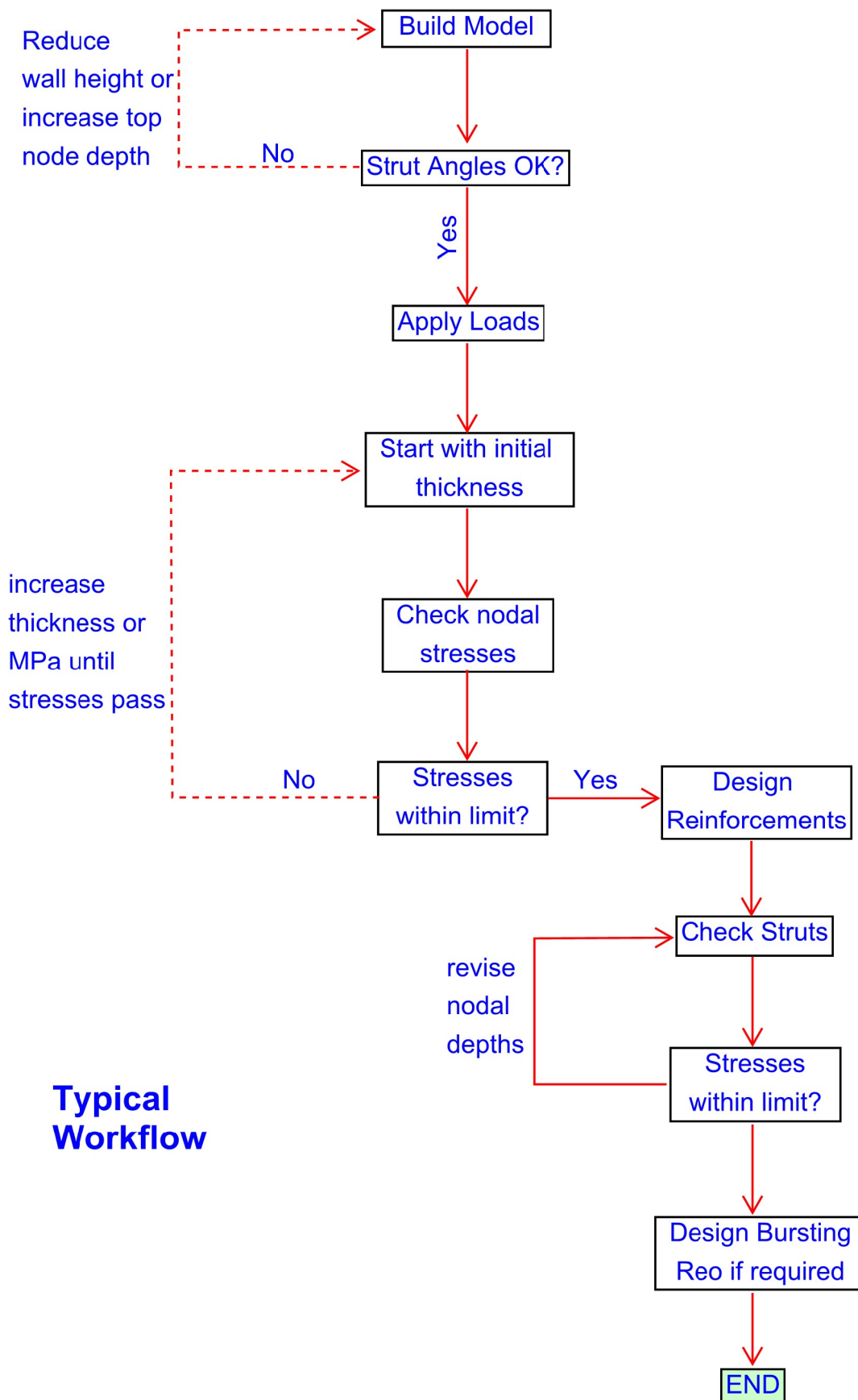
- 1- Nodes (being CCC, CCT, CTT)
- 2- Struts (Fan or uniform struts, including their inclination angles)
- 3- Rebar anchorage and stress limits



Theory

General rules to follow:

1. The concrete structure is basically divided into either B (Bernoulli) regions where the beam theory applies and stress distribution is linear within the section, or D (Disturbed) regions where it doesn't.
2. Within the D regions, truss analogy can be applied by following the load path lines (principal stresses) and representing them as straight struts (compression members - concrete) and ties (tension members - reinforcement) intersect in nodes (concrete)
3. The angle between diagonal Struts and horizontal line is feasible between 25° and 65°
4. Equilibrium must be maintained while developing the STM model, and concrete must not fail before the steel reinforcement yields
5. Tension is neglected in concrete, and forces in struts are uniaxial
6. Anchorage and detailing are essential
7. There is no exact STM model; however, there are poor and good models.
8. Struts can be categorized into prism, bottle, and fan
9. Nodes (concrete) are categorized into 4 types: CCC, CCT, CTT, TTT (C stands for compression, and T stands for tension):
10. Stresses within struts, ties, support and under load regions must be within allowable code limits.





Build Model

Inputs

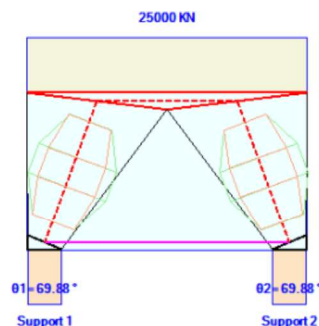
Materials	
f'_c (N/mm ²)	65
f_y (N/mm ²)	500
f_{ys} (N/mm ²)	250
Geometry (Units mm)	
Wall Height	5700
Wall Width	10000
Wall Thickness	350
Width of Applied Load	10000
Location of Applied Load	5000
Width of Support 1	1200
Width of Support 2	1200
Centre of Top Node	300
Centre of Bottom Nodes	250
Vertical Loads	
Ultimate (KN)	25000
Service (KN)	19230

[To Cloud](#) [ShareKALC](#)

Analysis & REO

Span/Depth	1.75
Reaction1	12500
Reaction2	12500
Tie Force	4579
REO mm ²	10775
Strut1 Force	13312
Strut1 Angle	69.9
Strut2 Force	13312
Strut2 Angle	69.9

Preview



5700 is the height that results in 70 degrees user may alter this if looking for less angle

Apply Loads

Nodes

[Top Node-Left](#) [Top Node-Right](#)

Nodal Stressess

Width (mm)	5000	Top Stress	7.14
Height (mm)	600	Side Stress	21.81
Hypo (mm)	5035.87	Incl. Stress	7.35
Strut/Node Angle	13.28	Shear Stress	1.73
Applied (MPa)	21.81	Allowed MPa	38.03

[Mohr Circle](#)

Left Node

Width (mm)	1200	Base Stress	29.76
Height (mm)	500	Side Stress	26.17
Hypo (mm)	1300	Incl. Stress	29.23
Strt./Nd. Ang	2.5	Shear Stress	1.28
Applied (MPa)	29.76	Allowed MPa	30.42

[Mohr Circle](#)

Right Node

Width (mm)	1200	Base Stress	29.76
Height (mm)	500	Side Stress	26.17
Hypo (mm)	1300	Incl. Stress	29.23
Strt./Nd. Ang	2.5	Shear Stress	1.28
Applied (MPa)	29.76	Allowed MPa	30.42

[Mohr Circle](#)



Non-Hydrostatic node with shear stress check



Design Reinforcements

10775 =
18N28

spread over 6 layers
of 3 bars

spread
rebar
over the
Node
depth

Anchor
reinforce
ment

See
standard

0.50 m

0.35 m

Analysis & REO

Span/Depth

1.75

Reaction1

12500

Reaction2

12500

Tie Force

4579

REO mm²

10775

Strut1 Force

13312

Strut1 Angle

69.9

Strut2 Force

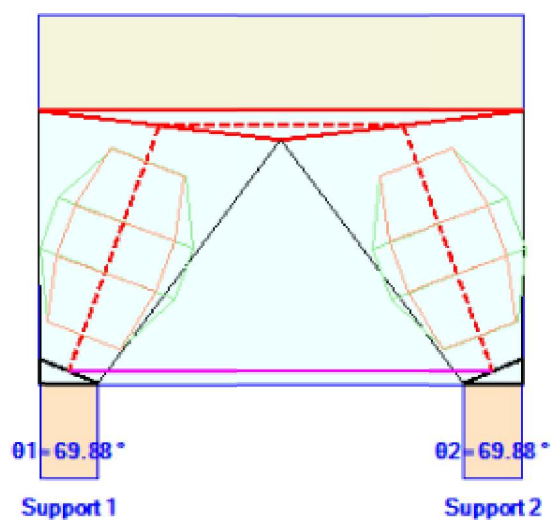
13312

Strut2 Angle

69.9

Preview

25000 kN





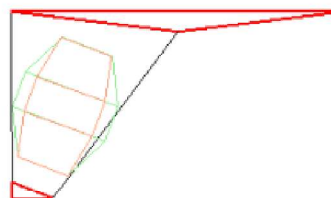
Check Struts

Left Strut

Min Width	1300
Max Width	5036
Average Dc (mm)	3168
Length	5378
Lb	2210
Strut Angle	69.88
Efficiency Factor	0.92
Strut Force KN	13312
Applied σ (MPa)	29.26
Allowed σ (MPa)	34.93
f_{ct} (MPa)	2.9
Tb,cr Bursting (KN)	1572
SLS* Burst. (KN)	5120
ULS* Burst. (KN)	2662
Hor.REO Total Both Faces mm	15963
Vert. REO Total Both Faces mm	15963
ULS Burst. Capacity	10240
SLS Burst. Capacity	5120

Strut Situation

OK

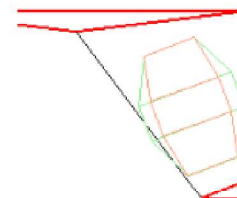


Right Strut

Min Width	1300
Max Width	5036
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Hor.REO Total Both Faces mm	15963
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ULS Burst. Capacity	10240
SLS Burst. Capacity	5120

Strut Situation

OK



Horizontal Reo
15963 =
7982 mm² per face

divide by height = 5.7
this becomes
1400mm²/m
Provide
N20-200=1570mm²

Vertical Reo
15963 =
7982 mm² per face

divide by span = 10
this becomes
799mm²/m
Provide
N16-200=1005mm²



STM Wall

Analysis & Nodes

Struts

Calculations

My Walls

Watch & Learn

Hello, RKALC !

You have 0 Messages

Your Design Package is valid until 30/03/2030 10:44:38 PM

Inputs

Materials

f_c (N/mm²)

f_y (N/mm²)

f_{ys} (N/mm²)

Geometry (Units mm)

Wall Height

Wall Width

Wall Thickness

Width of Applied Load

Location of Applied Load

Width of Support 1

Width of Support 2

Centre of Top Node

Centre of Bottom Nodes

Vertical Loads

Ultimate (KN)

Service (KN)

To Cloud

ShareKALC

RKALC Assistant New

Analysis & REO

Span/Depth

Reaction1

Reaction2

Tie Force

REO mm²

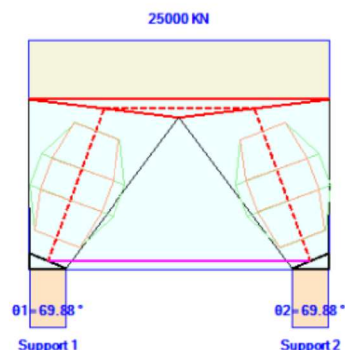
Strut1 Force

Strut1 Angle

Strut2 Force

Strut2 Angle

Preview



Nodes

Top Node-Left Top Node-Right

Width (mm)

Height (mm)

Hypo (mm)

Strut/Node Angle

Applied (MPa)

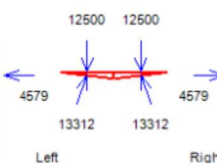
Top Stress

Side Stress

Incl. Stress

Shear Stress

Allowed MPa



Mohr Circle

Left Node

Width (mm)

Height (mm)

Hypo (mm)

Strt./Nd. Ang

Applied (MPa)

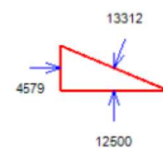
Base Stress

Side Stress

Incl. Stress

Shear Stress

Allowed MPa



Mohr Circle

Right Node

Width (mm)

Height (mm)

Hypo (mm)

Strt./Nd. Ang

Applied (MPa)

Base Stress

Side Stress

Incl. Stress

Shear Stress

Allowed MPa



Mohr Circle

RKALC Assistant

You: how is wall doing in your opinion?

RKALC: Based on the current wall analysis, the utilization of the left bottom node and right bottom node is at 98%, indicating high stress on these nodes. However, the utilization of the top node (both left half and right half) is at 57%, which is relatively lower. The required tie reinforcement is calculated to be 10775 sq.mm. The strut angles for both the left and right sides are at 69.9 degrees, indicating compliance with STM guidelines.

how is wall doing in your opinion?

Speak

Voice

Clear

Close





Introduction

This document provides analysis of non-flexural element design in accordance with the Australian Standard AS3600-2018. It covers both the ultimate and service conditions, addressing the following aspects:

- Flexural Reinforcement
- Nodal Stresses and compliance with the Standard
- Strut Checks, including bursting

The design ensures structural integrity and compliance with the standard under the specified loading conditions. For detailed guidelines and requirements, refer to the relevant sections of AS3600-2018-A2.

This calculation can be reproduced and checked independently. For more details, refer [RKALC website](http://www.rkalc.com).

Material Properties

Concrete Strength $f_c = 65$ MPa

Rebar $f_y = 500$ MPa

SLS Rebar stress $f_{ys} = 250$ MPa

Geometry

Wall Height = 5700 mm

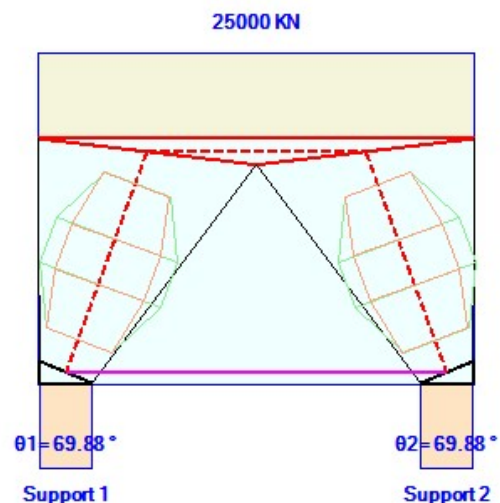
Wall Width = 10000 mm

Wall Thickness = 350 mm

Width of Left Support = 1200 mm

Width of Right Support = 1200 mm

Width of Applied Load = 10000 mm



Applied Loads

Ultimate Load = 25000 KN

Service Load = 19230 KN

Width of Applied Load = 10000 mm

Centre of Applied Load (from left edge of the wall) = 5000 mm

Nodal Assumptions

- Top Node

The node at the top is receiving the load, width of which equal to the node's width. Node is essentially divided into two triangulated nodes (left and right), these have widths constructed from the shares of load they take

Top Node Width (total) = 10000 mm

Top Node Depth = 600 mm

Node Thickness = 350 mm

- Left Node

Left Node Width = 1200 mm

Left Node Depth = 500 mm

Node Thickness = 350 mm

- Right Node

Right Node Width = 1200 mm

Right Node Depth = 500 mm

Node Thickness = 350 mm

Analysis and Required Reinforcement

Span-Depth Ratio of the STM Model = 1.75

Left Node Reaction = 12500 KN

Right Node Reaction = 12500 KN

Resulting Tie Force = 4579 KN

Required REO = 10775 mm²

Left Strut Force = 13312 KN

Left Strut Angle = 69.88 Degrees

Right Strut Force = 13312 KN

Right Strut Angle = 69.88 Degrees

Ensure the reinforcement is reasonable, not heavy. spread so the centre of bars is passing by the centre of the nodes at the bottom

Nodal Capacity Check

Top Node

- Left part

Width (Based on Share of Load Taken) = 5000 mm

Base stress = 350 N/mm²

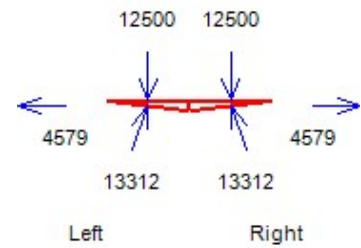
Side stress = 21.81 N/mm²

Inclined stress = 7.35 N/mm²

Shear stress = 1.73 N/mm²

Allowed Stress (CCC Node) = 38.03 N/mm²

Status = Pass



-
- Right part

Width (Based on Share of Load Taken) = 5000 mm

Base stress = 350 N/mm²

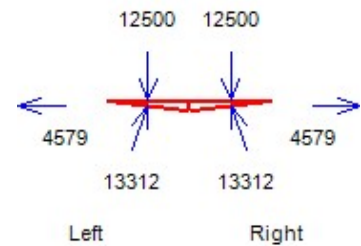
Side stress = 21.81 N/mm²

Inclined stress = 7.35 N/mm²

Shear stress = 1.73 N/mm²

Allowed Stress (CCC Node) = 38.03 N/mm²

Status = Pass



Bottom-Left node

Base stress = 29.76 N/mm²

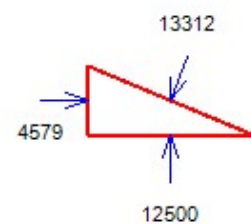
Side stress = 26.17 N/mm²

Inclined stress = 29.23 N/mm²

Shear stress = 1.28 N/mm²

Allowed Stress (CCT Node) = 30.42 N/mm²

Status = Pass



Bottom-Left node

Base stress = 29.76 N/mm²

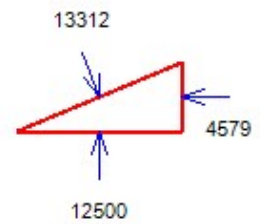
Side stress = 26.17 N/mm²

Inclined stress = 29.23 N/mm²

Shear stress = 1.28 N/mm²

Allowed Stress (CCT Node) = 30.42 N/mm²

Status = Pass



Left Strut

Average Dc = 3168 mm

Lb = 2210 mm

Angle = 69.88 Degrees

Efficiency Factor = 0.92

Applied MPa = 29.26

Allowed MPa = 34.93

fct = 2.9 MPa

Tb,cr Bursting = 1572 MPa

SLS* Bursting = 5120 KN

ULS* Burst = 2662 KN

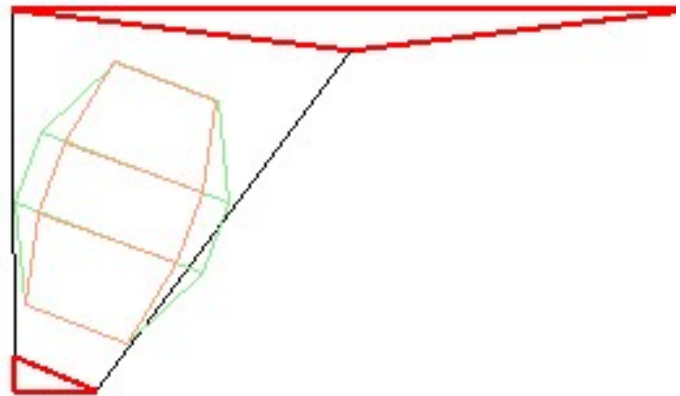
Hor.REO Total Both Faces mm = 15963
mm²

Vert.REO Total Both Faces mm = 15963
mm²

ULS Burst. Capacity = 10240 KN

SLS Burst. Capacity = 5120 KN

Strut Status = OK



Left Strut

Average Dc = 3168 mm

Lb = 2210 mm

Angle = 69.88 Degrees

Efficiency Factor = 0.92

Applied MPa = 29.26

Allowed MPa = 34.93

fct = 2.9 MPa

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mm²

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SLS Burst. Capacity = 5120 KN

Strut Status = OK

