



Sample Structure - to be analysed using FeaKALC 3D

INTRODUCTION

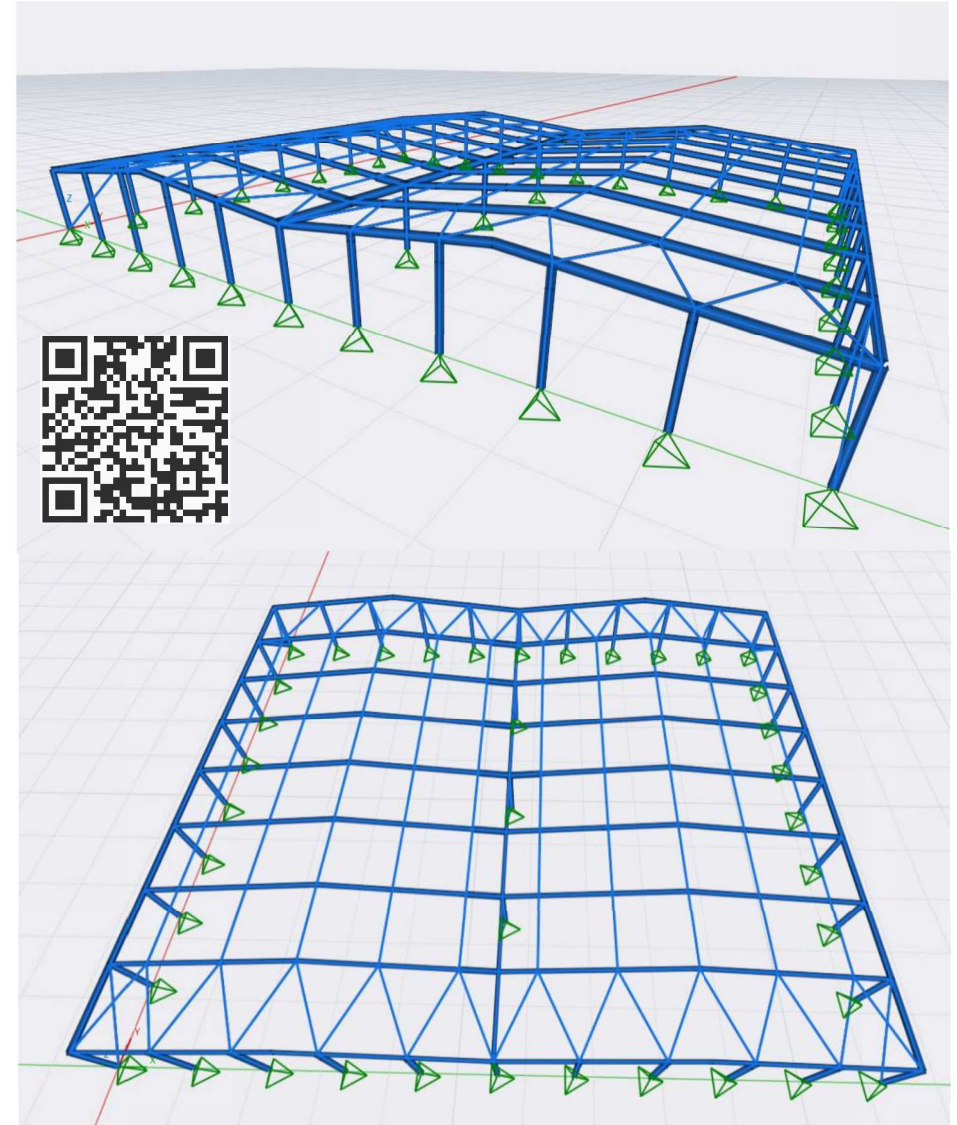
THIS TUTORIAL DEMONSTRATES THE MODELLING, LOADING, ANALYSIS AND DESIGN VERIFICATION OF A TYPICAL STEEL WAREHOUSE STRUCTURE USING FEAKALC 3D. THE OBJECTIVE OF THE TUTORIAL IS NOT ONLY TO DEMONSTRATE THE SOFTWARE WORKFLOW, BUT ALSO TO ILLUSTRATE THE ENGINEERING CONSIDERATIONS INVOLVED IN DEVELOPING A STRUCTURAL ANALYSIS MODEL SUITABLE FOR DESIGN TO AUSTRALIAN STANDARDS.

THE EXAMPLE STRUCTURE CONSISTS OF A MULTI-SPAN STEEL PORTAL FRAME WAREHOUSE WITH COLD-FORMED STEEL PURLINS AND SIDE GIRTS SUPPORTING LIGHTWEIGHT ROOF AND WALL CLADDING. THE STRUCTURE IS SUBJECTED TO GRAVITY AND WIND ACTIONS IN ACCORDANCE WITH AS/NZS 1170.

THE TUTORIAL SERIES WILL COVER:

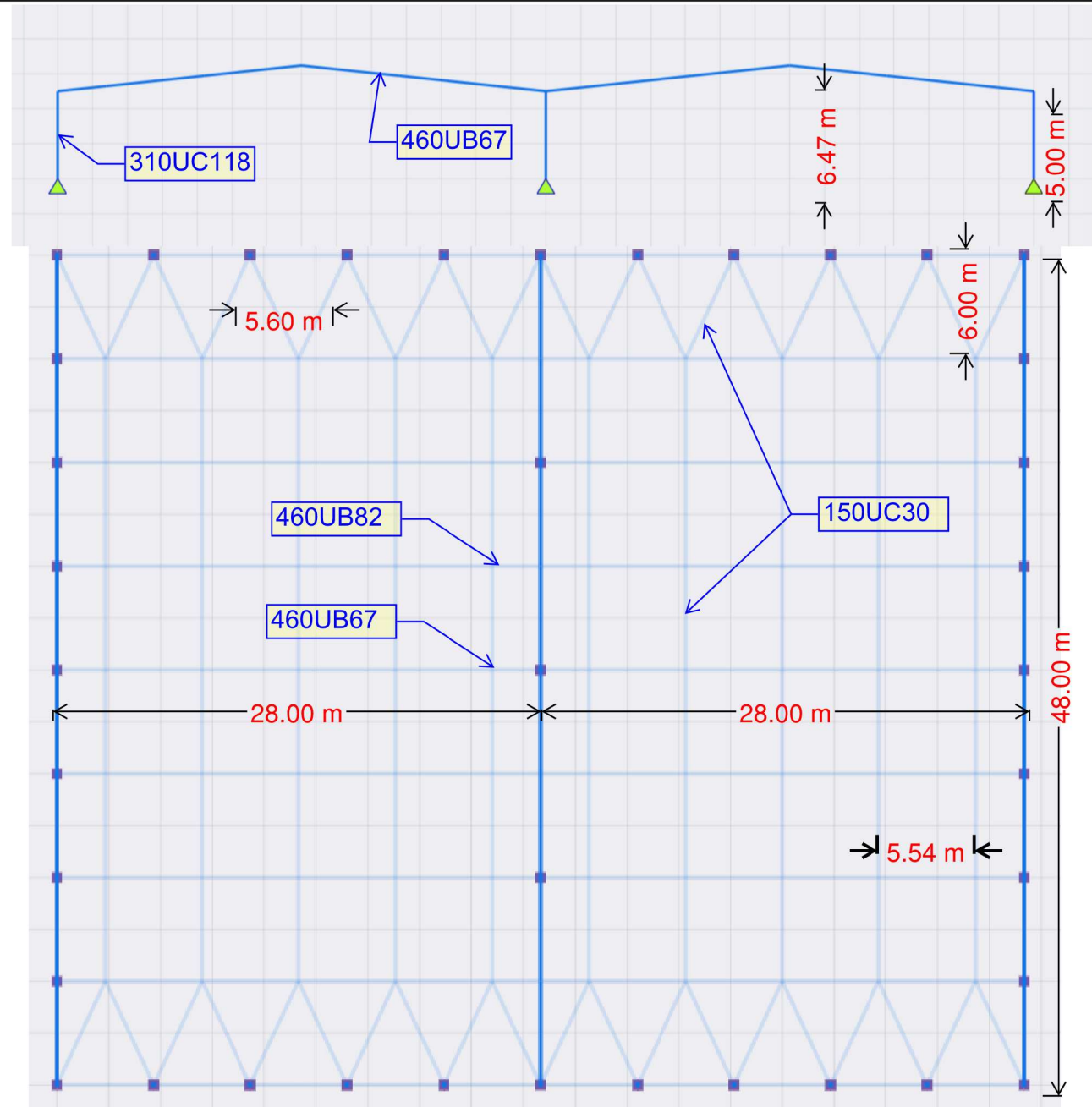
- DEVELOPMENT OF THE STRUCTURAL MODEL GEOMETRY
- DEFINITION OF MATERIAL AND SECTION PROPERTIES
- DETERMINATION OF GRAVITY LOADS
- DETERMINATION OF WIND LOADS IN ACCORDANCE WITH AS/NZS 1170.2
- APPLICATION OF LOAD CASES AND LOAD COMBINATIONS
- LINEAR ELASTIC ANALYSIS USING FEAKALC 3D
- INTERPRETATION OF REACTIONS, MEMBER FORCES AND DEFLECTIONS
- DESIGN VERIFICATION OF PRIMARY STEEL MEMBERS TO AS 4100

THE CALCULATIONS AND LOAD ASSUMPTIONS PRESENTED HEREIN ARE INTENDED FOR EDUCATIONAL PURPOSES AND TO DEMONSTRATE THE MODELLING PROCESS. ENGINEERS SHOULD ALWAYS EXERCISE PROFESSIONAL JUDGEMENT AND VERIFY ALL ASSUMPTIONS, LOADING CRITERIA AND DESIGN REQUIREMENTS APPLICABLE TO THEIR SPECIFIC PROJECT. THIS TUTORIAL FORMS PART OF THE RKALC LEARNING CENTRE, WHICH PROVIDES PRACTICAL ENGINEERING EXAMPLES AND TRAINING RESOURCES FOR STRUCTURAL ENGINEERS USING THE RKALC ECOSYSTEM.





Geometry





Gravity Loads

A - Dead Loads

1 - Roof Sheeting = 5 kg/m²

2 - Own Weight of Steel Beams

- UB's at 67kg/m', spaced at 6 meters

Weight = 67/6 = 11.17 kg/m² (this will be automatically included in FeaKALC)

3- Purlins

- say 150 Deep purlins at spacing = 1.2, weight of purlin = 3kg/m

- Loading becomes = 3/1.2 = 2.5kg/m²

4- Insulation

say 2 kg/m²

5- Services

say 30 kg/m²

5- False Ceiling

say 10 kg/m²

Total Dead load = 5 + 2.5 + 2 + 30 + 10 = 49.5 kg/m²

= 0.5 kN/m² (kPa) + own weight

**SEE
AS1170.1**

B- Live Load

Area of roof = 48x56 = 2688m²

= **0.25 kPa** (ref Table 3.2 below of AS1170.1 - 2002)

TABLE 3.2
REFERENCE VALUES OF ROOF ACTIONS

	Type of activity/occupancy for part of the building or structure	Specific uses	Uniformly distributed actions	Concentrated actions
			kPa	kN
A2	R1 Street awnings (including cladding)	Accessible from adjacent windows, roofs or balconies	1.5	1.8
		Accessible only from ground level	1.0	1.8
	R2 Other roofs	(i) Structural elements	(1.8/A + 0.12) but not less than 0.25 (see Notes 1, 2 and 3)	1.4 (see Note 3)
		(ii) Cladding providing direct support	As for structural elements	1.1
		(iii) Surfaces over which boards or ladders are required to be laid	—	0.5

NOTES:

1 Structural elements supporting more than 200 m² of roof area shall be designed to support 0.25 kPa on the 200 m² of the supported area that gives the worst effect.

2 A = the plan projection of the surface area of roof supported by the member under analysis, in square metres.

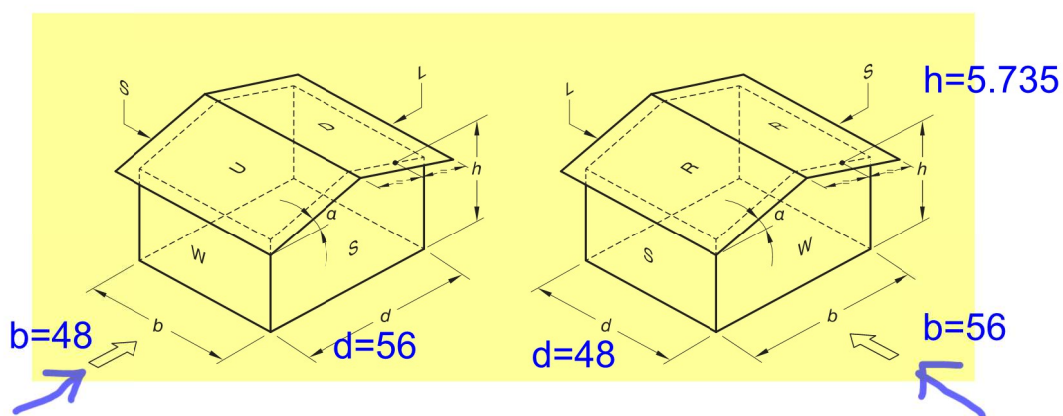
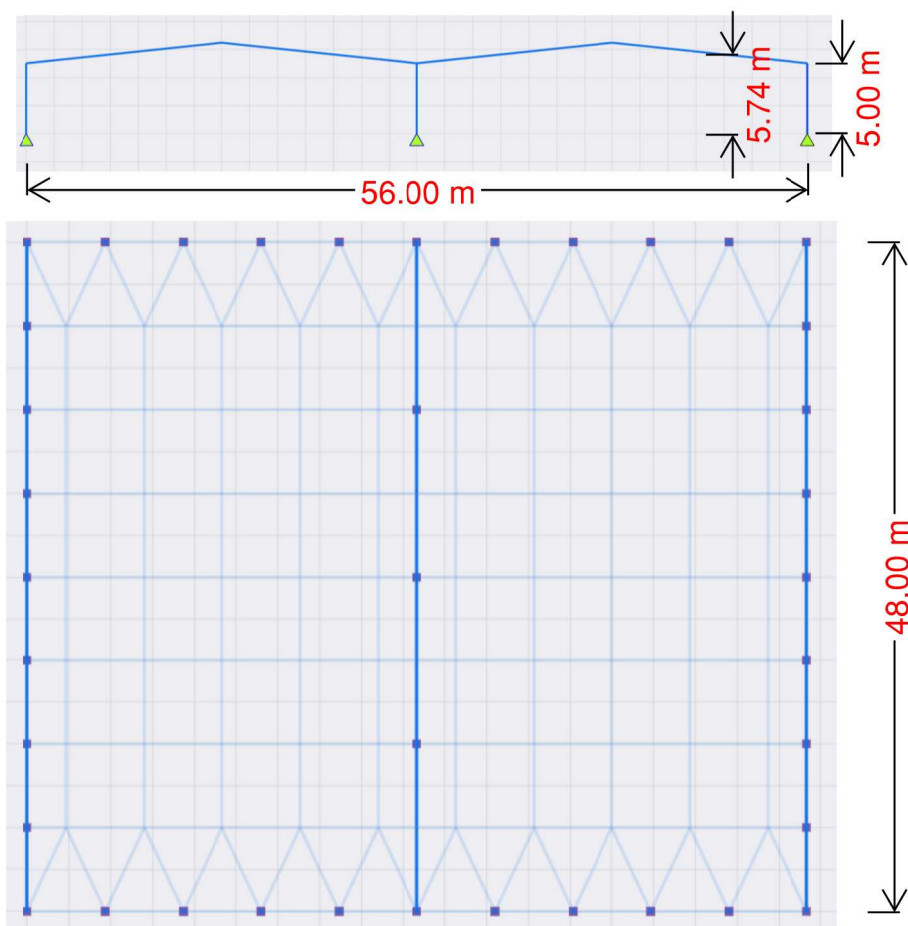
A2 3 For structural elements in roofs of houses, the uniform distributed actions shall be 0.25 kPa and the concentrated actions shall be 1.1 kN.



Wind Loads

Basic Wind Pressure = $0.6 \times 45^2 \times C_{fig} = 1.215 \times C_{fig}$

SEE
AS1170.2



Cross Wind Case

$\alpha = 6$ degrees
 $h/d = 5.735/56 = 0.1 < 0.5$
 $d/b = 56/48 = 1.16 > 1$

Along Wind Case

$\alpha = 6$ degrees
 $h/d = 5.735/48 = 0.12 < 0.5$
 $d/b = 48/56 = 0.857$



Wind Loads

Reference tables

Table 5.2(A) — Walls — External pressure coefficients ($C_{p,e}$) for rectangular enclosed buildings — Windward wall (W)

h	External pressure coefficients ($C_{p,e}$)
> 25.0 m	0.8 (wind speed varies with height)
≤ 25.0 m	For buildings on ground—
	0.8, when wind speed varies with height; or
	0.7, when wind speed is taken for $z = h$
	For elevated buildings—
	0.8 (wind speed taken at h)

Table 5.2(B) — Walls — External pressure coefficients ($C_{p,e}$) for rectangular enclosed buildings — Leeward wall (L)

Wind direction θ degrees (see Figure 2.2)	Roof shape	Roof pitch (α), degrees	d/b	External pressure coefficients ($C_{p,e}$)
0	Hip or gable	< 10	≤ 1	-0.5
			2	-0.3
			≥ 4	-0.2
0	Hip or gable	10	All values	-0.3
				-0.3
				-0.4
0	Hip or gable	15	All values	-0.3
				-0.3
				-0.4
0	Hip or gable	20	All values	-0.3
				-0.3
				-0.4
0	Hip or gable	≥ 25	≤ 0.1	-0.75
			≥ 0.3	-0.5
			≥ 4	-0.2
90	Gable (see Note 3)	All values	≤ 1	-0.5
			2	-0.3
			≥ 4	-0.2

NOTE 1 For intermediate values of d/b and α , linear interpolation should be used.

NOTE 2 The design wind speed to be used with these pressure coefficients should be taken at the average roof height ($z = h$).

NOTE 3 For hip roofs use the same values as for $\theta = 0^\circ$.

Table 5.2(C) — Walls — External pressure coefficients ($C_{p,e}$) for rectangular enclosed buildings — Side walls (S)

Horizontal distance from windward edge	External pressure coefficients ($C_{p,e}$)
0 to 1h	-0.65
1h to 2h	-0.5
2h to 3h	-0.3
> 3h	-0.2

NOTE The design wind speed to be used with these pressure coefficients should be taken at the average roof height ($z = h$).

Table 5.3(A) — Roofs — External pressure coefficients ($C_{p,e}$) for rectangular enclosed buildings — For upwind slope (U), and downwind slope (D) and (R) for gable roofs with $\alpha < 10^\circ$, and monoslope roofs

Roof type and slope		Horizontal distance from windward edge of roof	External pressure coefficient ($C_{p,e}$)	
Crosswind slopes for gable roofs, and downwind slopes of monoslope roofs (R)	Upwind slope (U), downwind slope (D)		$h/d \leq 0.5$	$h/d \geq 1.0$
All α	$\alpha < 10^\circ$	0 to 0.5h	-0.9, -0.4	-1.3, -0.6
		0.5 to 1h	-0.9, -0.4	-0.7, -0.3
		1h to 2h	-0.5, 0	(-0.7), (-0.3)
		2h to 3h	-0.3, 0.1	See NOTE
		> 3h	-0.2, 0.2	

NOTE The values given in parentheses are provided for interpolation purposes.

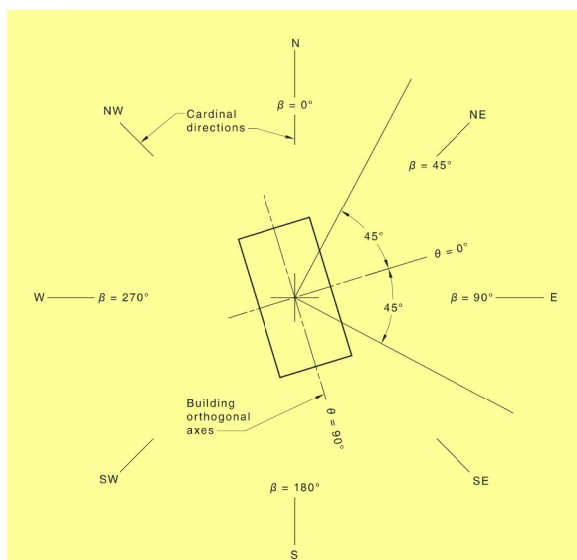
Table 5.1(B) — Internal pressure coefficients ($C_{p,i}$) for buildings with openings greater than 0.5 % of the area of the corresponding wall or roof

Ratio of area of openings on one surface to the sum of the total open area (including permeability) of other wall and roof surfaces	Largest opening on windward wall	Largest opening on leeward wall	Largest opening on side wall	Largest opening on roof
0.5 or less	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0
1	-0.1, 0.2	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0
2	$0.7 K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$
3	$0.85 K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$
6 or more	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$	$K_a K_\ell C_{p,e}$

NOTE 1 $C_{p,e}$ is the relevant external pressure coefficient at the location of the largest opening. For example, in Column 2, $C_{p,e}$ means the windward wall pressure coefficient obtained from Table 5.2(A); in Column 3, $C_{p,e}$ means the leeward wall pressure coefficient obtained from Table 5.2(B); in Column 5, $C_{p,e}$ means the roof pressure coefficient for that part of the roof containing the opening.

NOTE 2 K_a is the area reduction factor related to the total area of the opening(s), A , on the surface under consideration treating the "tributary area" as the area of the opening. See Clause 5.4.2.

NOTE 3 K_ℓ is the local pressure factor, based on the area and location of the opening on the surface under consideration, treating the "Area, A " as the area of the opening. See Clause 5.4.4.



**TABLE C1
EXTERNAL PRESSURE COEFFICIENTS ($C_{p,e}$) FOR
MULTI-SPAN BUILDINGS—PITCHED ROOFS**

Surface reference (see Figure C1)				
A	B	C	M	Y
0.7	Use Table 5.3(a), 5.3(b) or 5.3(c) for same (h/d) and α , as appropriate		-0.3 and 0.2 for $\alpha < 10^\circ$ -0.5 and 0.3 for $\alpha \geq 10^\circ$	-0.2

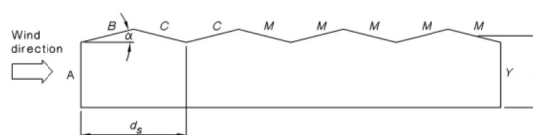


FIGURE C1 EXTERNAL PRESSURE COEFFICIENTS ($C_{p,e}$) FOR MULTI-SPAN BUILDINGS—PITCHED ROOFS

Table 5.2(C) — Walls — External pressure coefficients (C_{pe}) for rectangular enclosed buildings — Side walls (S)

Horizontal distance from windward edge	External pressure coefficients (C_{pe})
0 to 1h	-0.65
1h to 2h	-0.5
2h to 3h	-0.5
> 3h	-0.4

NOTE: The design wind speed to be used with these pressure coefficients should be taken at the average roof height ($z \pm h$).



Wind Loads - CASE 2

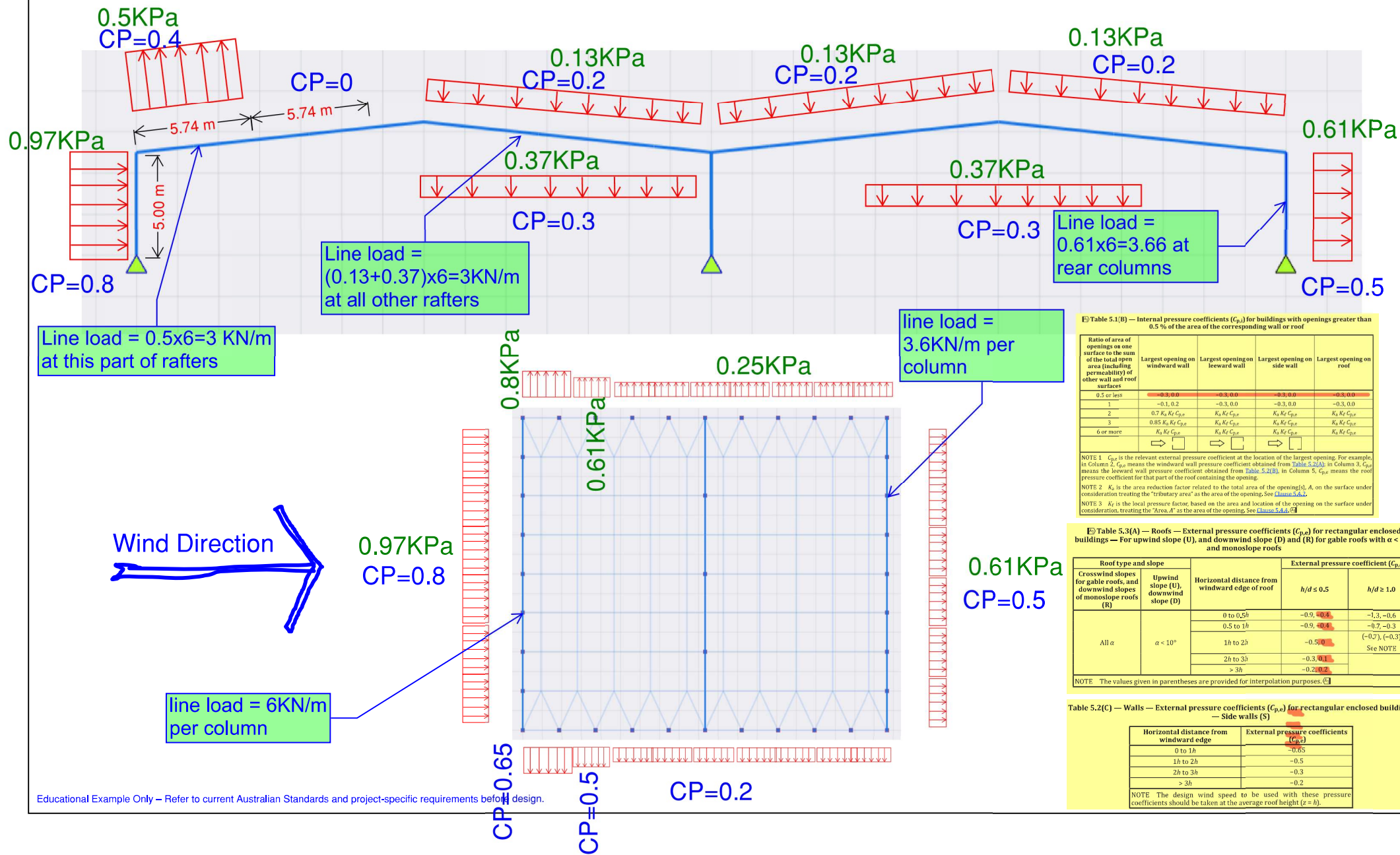


Table 5.1(B) — Internal pressure coefficients (C_{pi}) for buildings with openings greater than 0.5 % of the area of the corresponding wall or roof

Ratio of area of openings on one surface to the sum of the total open area (including permeability) of other wall and roof surfaces	Largest opening on windward wall	Largest opening on leeward wall	Largest opening on side wall	Largest opening on roof
0.5 or less	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0
1	-0.1, 0.2	-0.3, 0.0	-0.3, 0.0	-0.3, 0.0
2	$0.7 K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$
3	$0.85 K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$
6 or more	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$	$K_f K_t C_{pe}$

NOTE 1 C_{pe} is the relevant external pressure coefficient at the location of the largest opening. For example, in Column 2, C_{pe} means the windward wall pressure coefficient obtained from Table 5.2(A); in Column 3, C_{pe} means the leeward wall pressure coefficient obtained from Table 5.2(B); in Column 5, C_{pe} means the roof pressure coefficient for that part of the roof containing the opening.

NOTE 2 K_f is the area reduction factor related to the total area of the opening(s), A , on the surface under consideration treating the "tributary area" as the area of the opening. See Clause 5.4.4.

NOTE 3 K_t is the local pressure factor, based on the area and location of the opening on the surface under consideration, treating the "tributary area" as the area of the opening. See Clause 5.4.4.

Table 5.3(A) — Roofs — External pressure coefficients (C_{pe}) for rectangular enclosed buildings — For upwind slope (U), and downwind slope (D) and (R) for gable roofs with $\alpha < 10^\circ$, and monoslope roofs

Roof type and slope	Upwind slope (U), downwind slope (D)	Horizontal distance from windward edge of roof	External pressure coefficient (C_{pe})
All α	$\alpha < 10^\circ$	0 to 0.5h	-0.9, -0.4
		0.5 to 1h	-0.9, -0.4
		1h to 2h	-0.5, 0
		2h to 3h	-0.3, 0.1
		> 3h	-0.2, 0.2

NOTE: The values given in parentheses are provided for interpolation purposes.

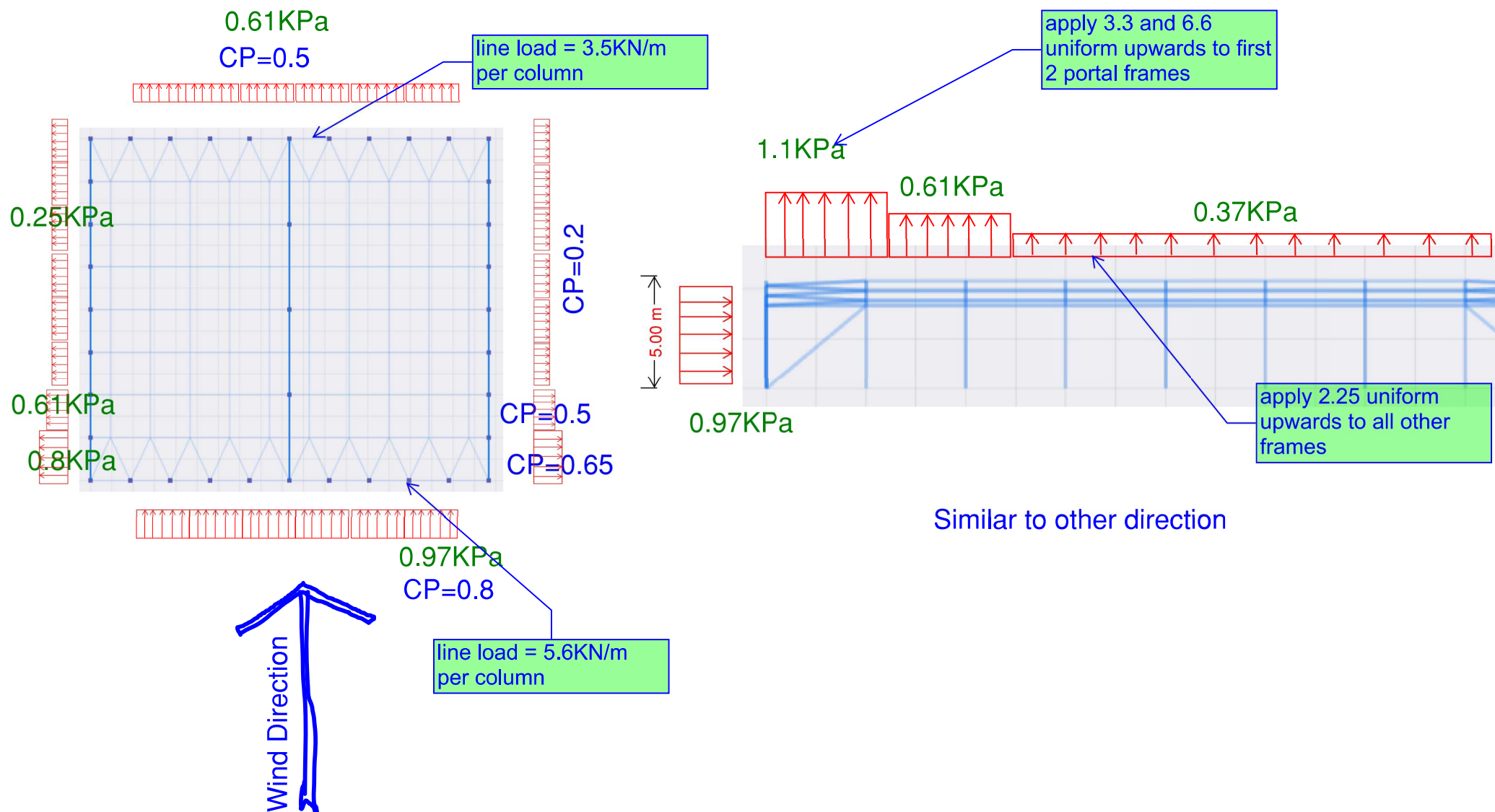
Table 5.2(C) — Walls — External pressure coefficients (C_{pe}) for rectangular enclosed buildings — Side walls (S)

Horizontal distance from windward edge	External pressure coefficients (C_{pe})
0 to 1h	-0.65
1h to 2h	-0.5
2h to 3h	-0.3
> 3h	-0.2

NOTE: The design wind speed to be used with these pressure coefficients should be taken at the average roof height ($z = h$).

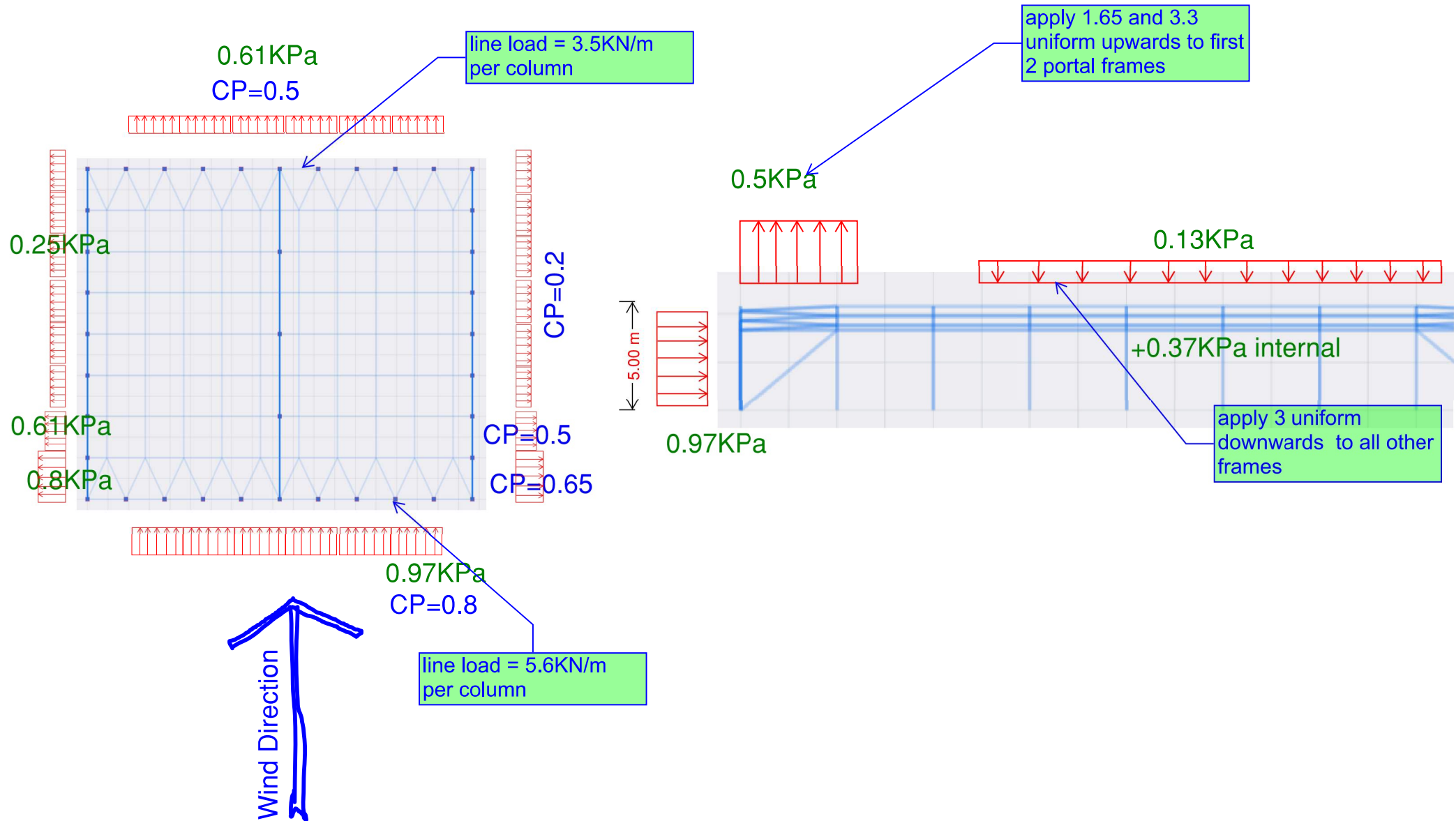


Wind Loads - CASE 3



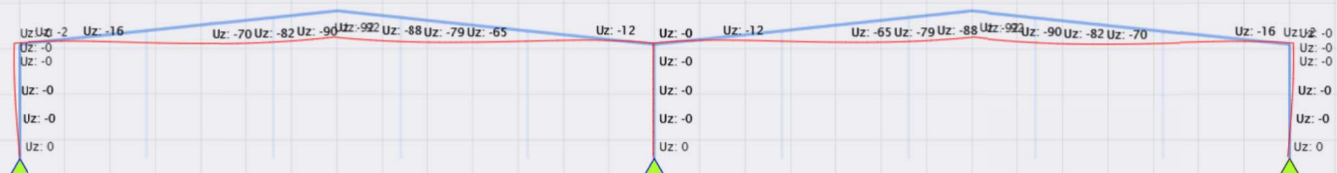


Wind Loads - CASE 4

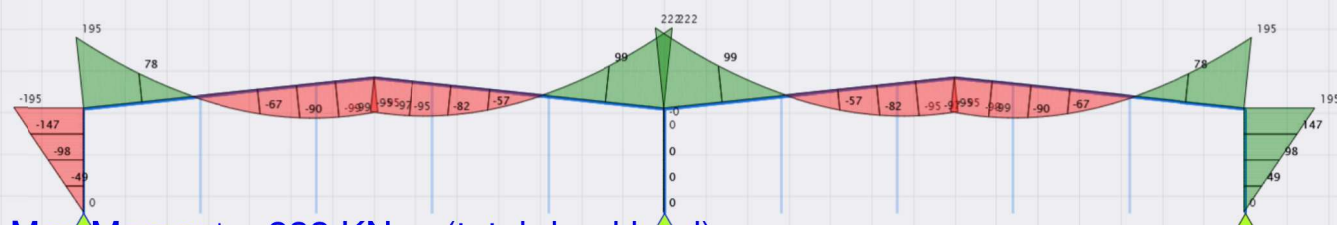
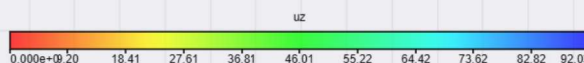




Initial Results



Max Deflection = 92 mm (total dead load)



Max Moment = 222 KN.m (total dead load)

for dead load, per beam = 3.67KN/m

Approx eve moment = $3.67 \times 28^2 / 14 = 205$ (not full fixity)

Deflection = 92 mm = $28000 / 305$ (Span/305)

dead load deflection is broken as follows

1-beam's own weight deflection = $0.67 / 3.67 \times 92 = 17$ mm

2- SDL deflection = $92 - 17 = 75$ mm

SDL deflection is broken down as follows

Roofing and insulation etc = $9.5\text{kg} / 49.5\text{total} = 19\% = 14.25$ mm

false ceiling and services = 81%

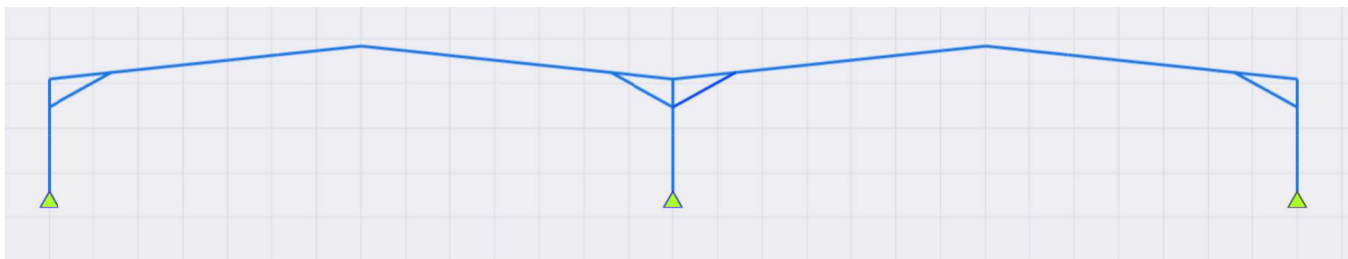
this means we can pre- camber by $14.25 + 17 = 32$ mm = 34% of dead load def.

net deflection = 60 (from other sustained loads).

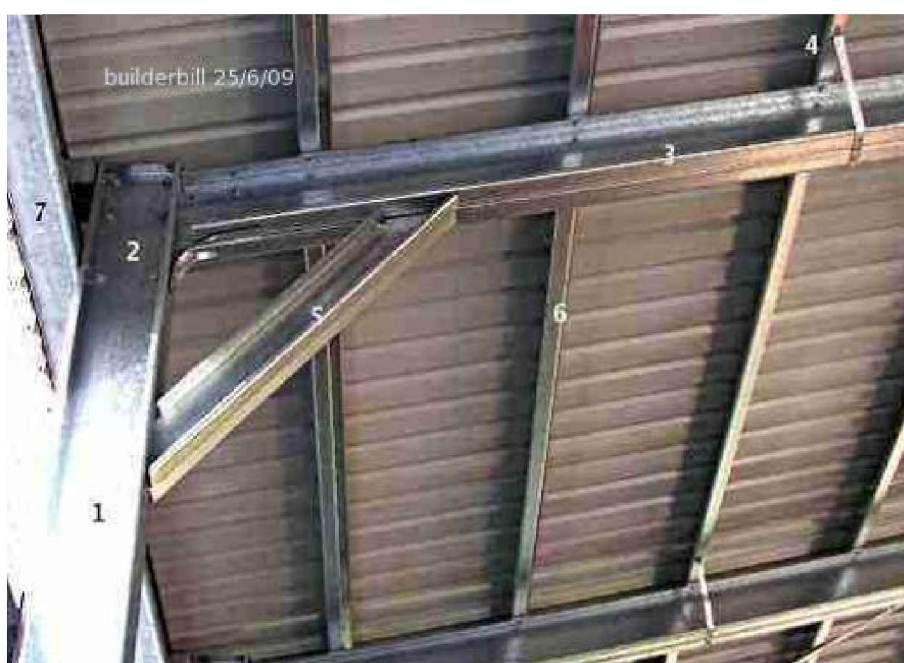
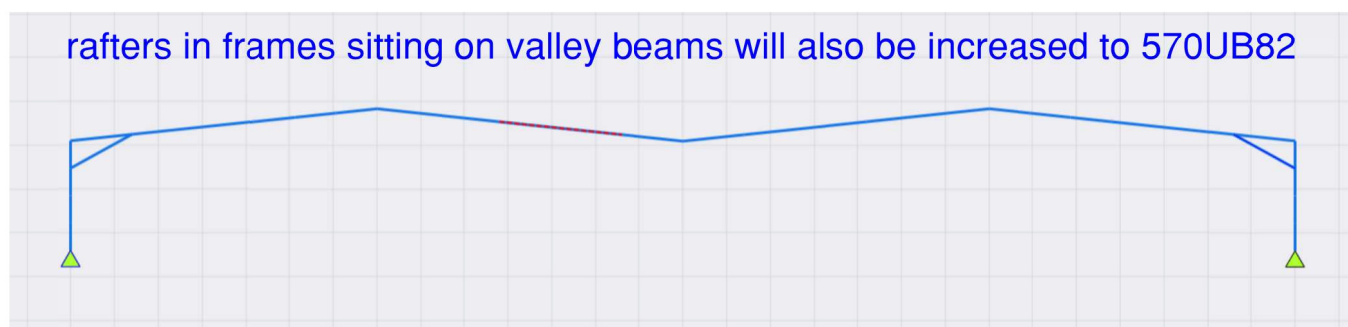


Potential Problems?

if false ceiling or services have no tolerance for 60 mm deflection (for example warehouse is going to be an office) then, we will need to add knee braces as follows:

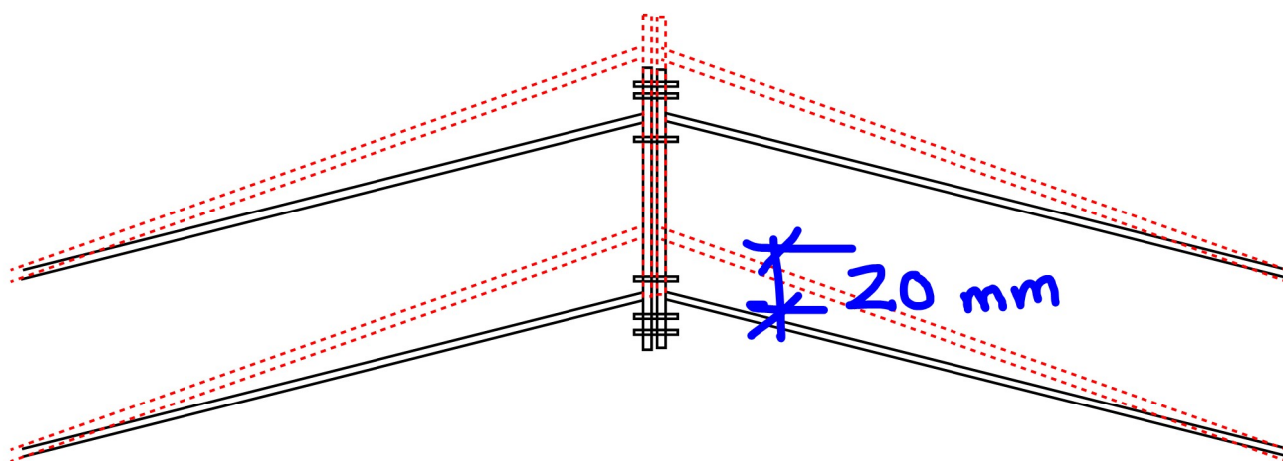
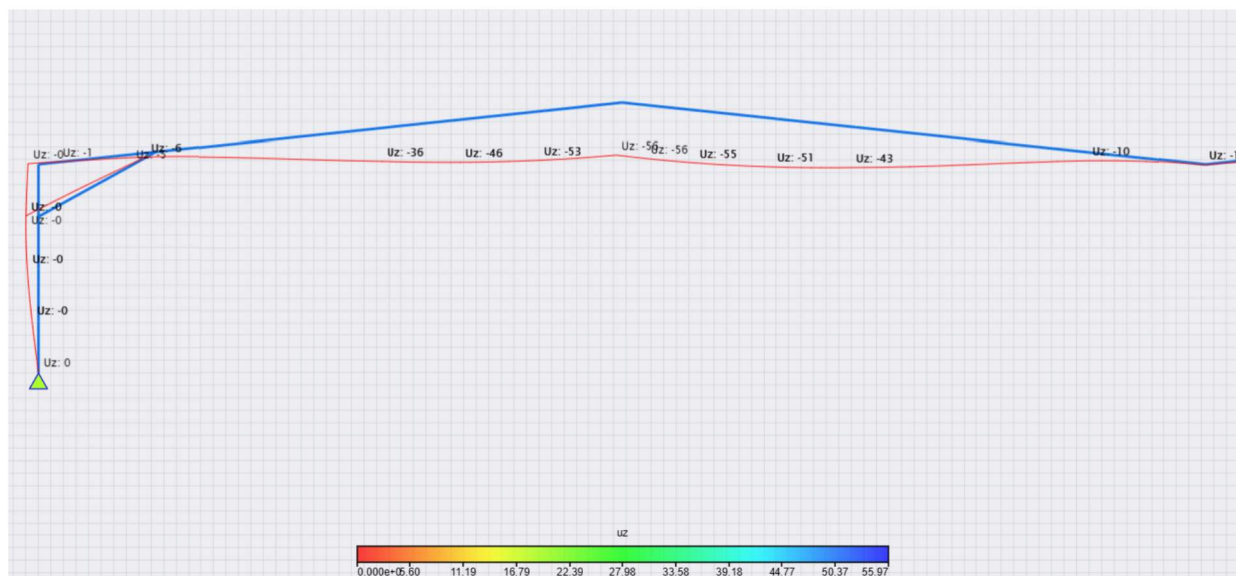


rafters in frames sitting on valley beams will also be increased to 570UB82





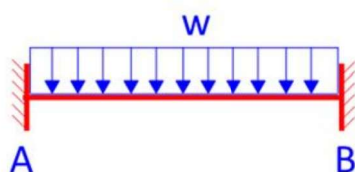
this will reduce dead load deflection to 53 mm, apply precamber = 30%
preamber = 16 mm, say 20 mm to be adopted



Preamber, this will essentially cancel deflection
caused by steel own weight, sheeting and purlins



How to Verify?



$$M_A = M_B = \frac{WL^2}{12}$$

$$M_{Midspan} = \frac{WL^2}{24}$$

$$\Delta = \frac{WL^4}{384EI}$$

$$R_A = R_B = \frac{WL}{2}$$

Support Moment (DL) =
 $WL^2 / 12 = 3.67 * 28^2 / 12 = 240 \text{ KN.m}$

Midspan Moment (DL) = 120

Deflection = $WL^4 / 384 / E / I = 99 \text{ mm}$

I Sections

Geometry

Steel Grade	300
Section Family	UB
Section	460UB67.1
Length - Axis X (mm)	2000
Length - Axis Y (mm)	2000



Key Properties

fy (N/mm²)	300	fu (N/mm²)	440
Class (X)	Compact	Class (Y)	Compact
Ze (X)	1480000	Ze (Y)	228947

Section Properties

Depth	454	Width	190
tw	8.5	tf	12.7
Weight (kg/m)	67.35	Area	8580
Ix	2.96E+08	Iy	1.45E+07
Zx	1303965	Zy	152631.6
Sx	1480000	Sy	238000
rx	185.7386	ry	41.10933
Iw	7.06E+11	J	378000

Model

Simplified

End Moment

~ 200

240 (fully fixed)

Midspan

~ 99

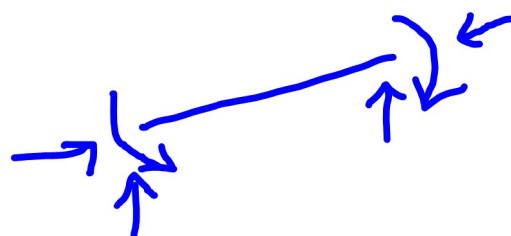
~ 120 (fully fixed)

Deflection

~ 93

~ 99 (fully fixed)

NOTE: members not flat, therefore axial forces reduce deflections and mess up approx calc





LEARNING
CENTRE



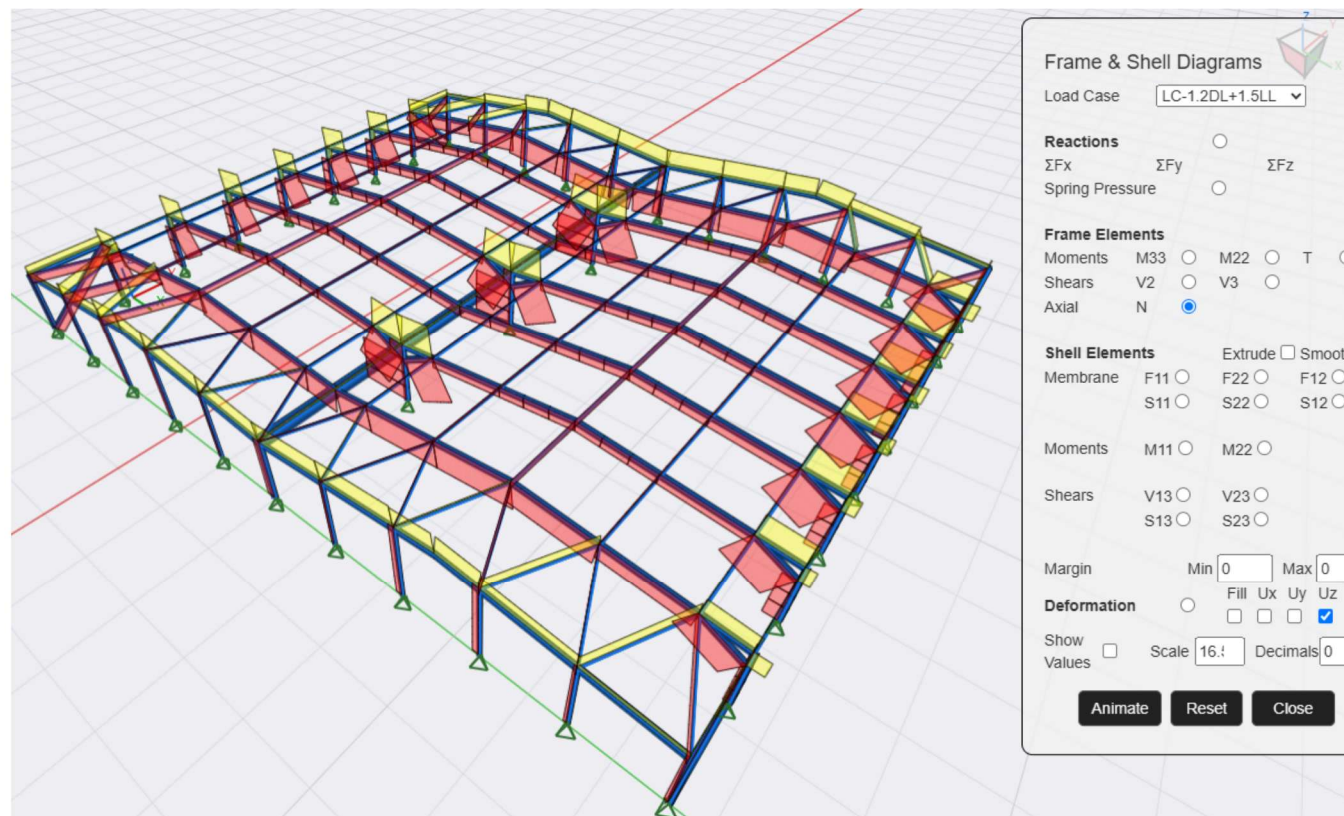
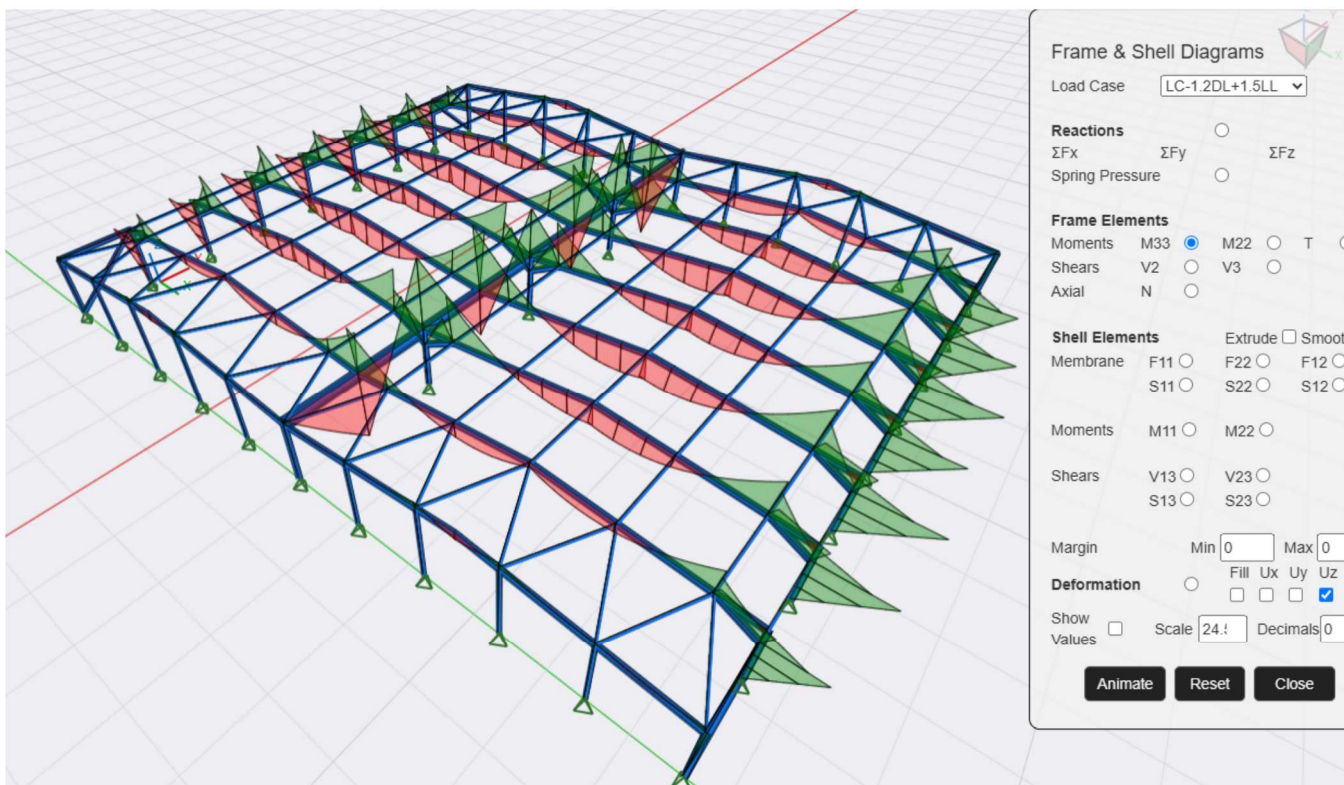
FeaKALC 3D Tutorial # 1

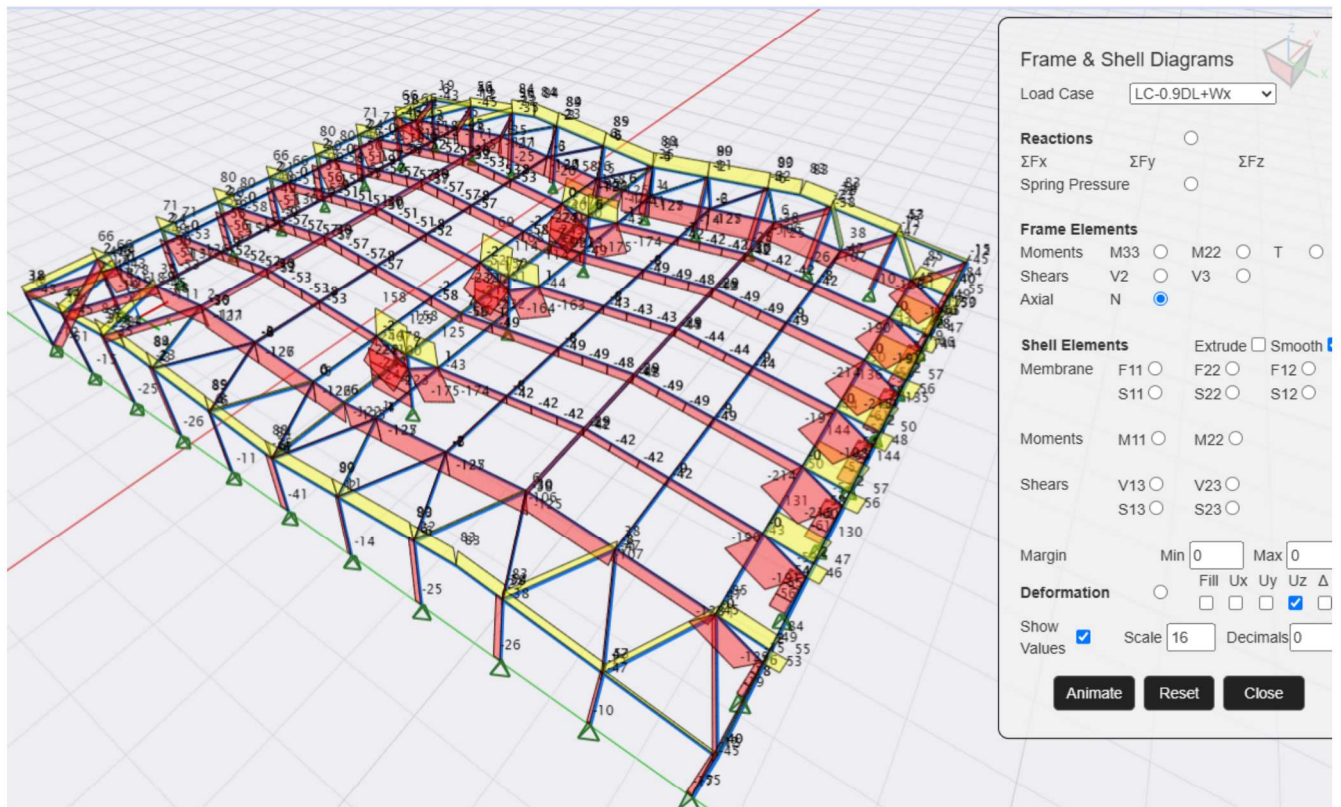
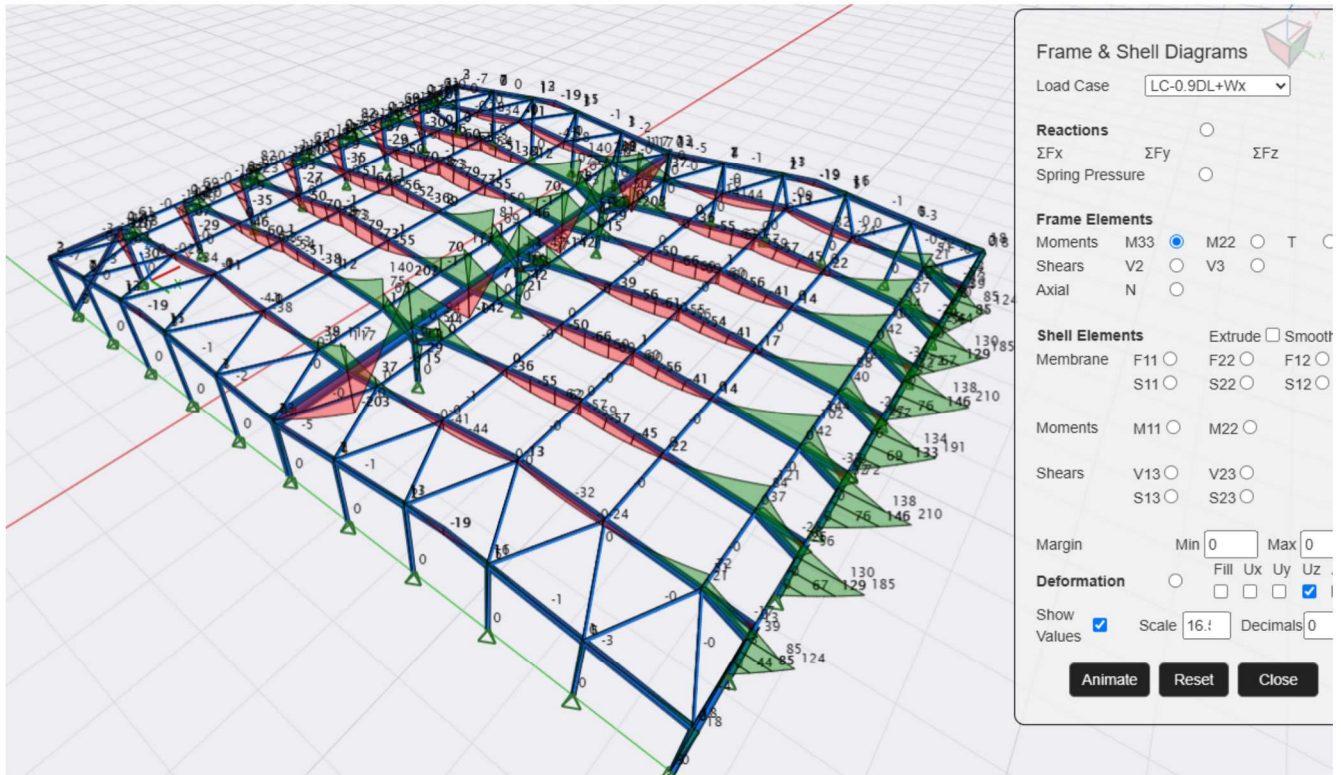
Warehouse to AS4100

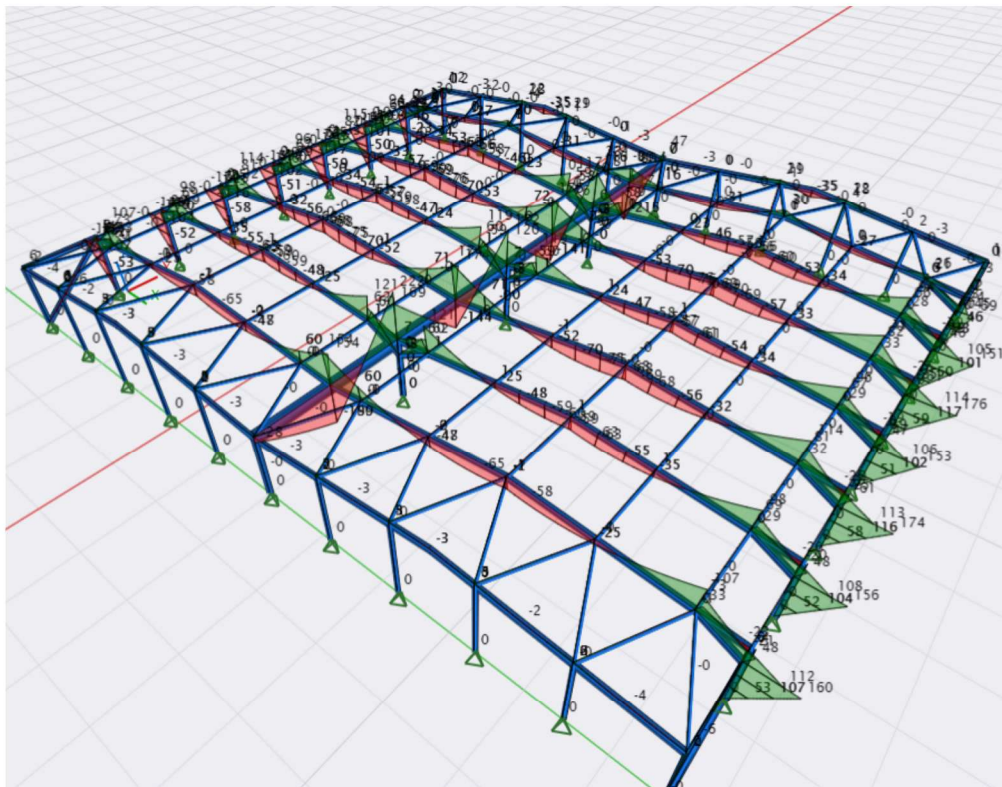
Sheet No.

Date

OUTPUT RESULTS







Frame & Shell Diagrams

Load Case: **LC-0.9DL+W_y**

Reactions

ΣF_x ΣF_y ΣF_z

Spring Pressure

Frame Elements

Moments: M33 ☒ M22 ☐ T ☐

Shears: V2 ☐ V3 ☐

Axial: N ☐

Shell Elements

Extrude ☐ Smooth ☐

Membrane: F11 ☐ F22 ☐ F12 ☐

S11 ☐ S22 ☐ S12 ☐

Moments: M11 ☐ M22 ☐

Shears: V13 ☐ V23 ☐

S13 ☐ S23 ☐

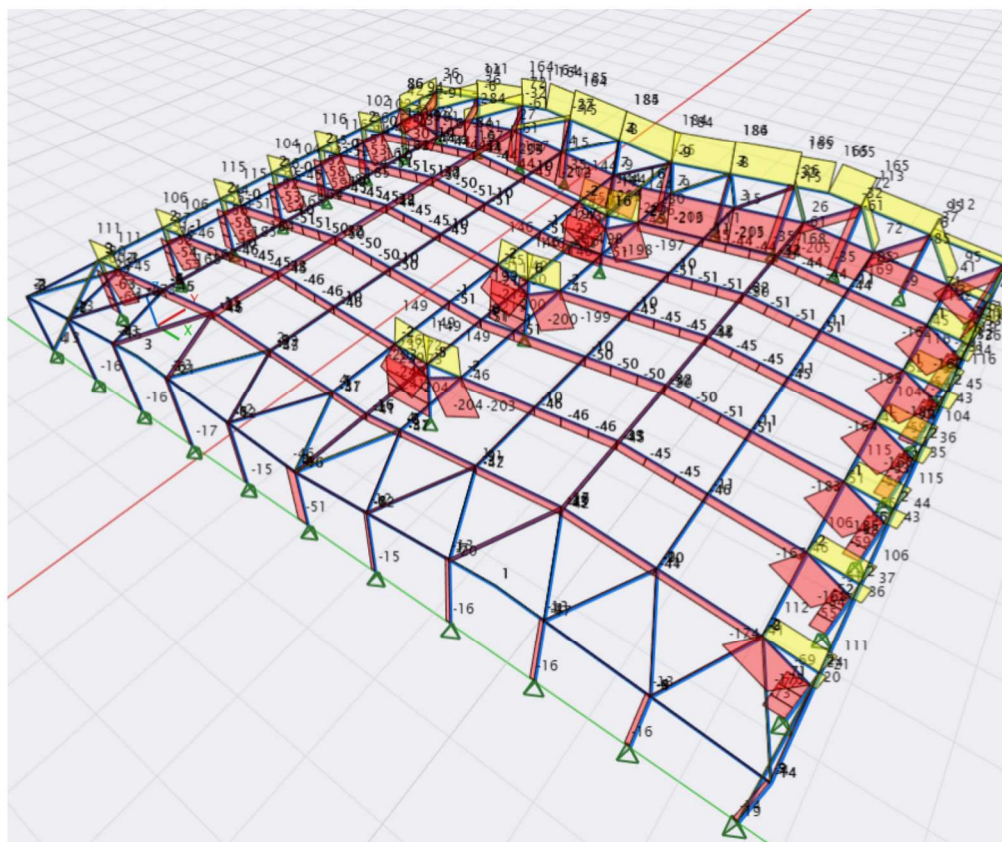
Margin: Min Max

Deformation

Fill Ux ☐ Uy ☐ Uz ☒

Show Values ☒ Scale: Decimals:

Animate **Reset** **Close**



Frame & Shell Diagrams

Load Case: **LC-0.9DL+W_y**

Reactions

ΣF_x ΣF_y ΣF_z

Spring Pressure

Frame Elements

Moments: M33 ☐ M22 ☐ T ☐

Shears: V2 ☐ V3 ☐

Axial: N ☒

Shell Elements

Extrude ☐ Smooth ☐

Membrane: F11 ☐ F22 ☐ F12 ☐

S11 ☐ S22 ☐ S12 ☐

Moments: M11 ☐ M22 ☐

Shears: V13 ☐ V23 ☐

S13 ☐ S23 ☐

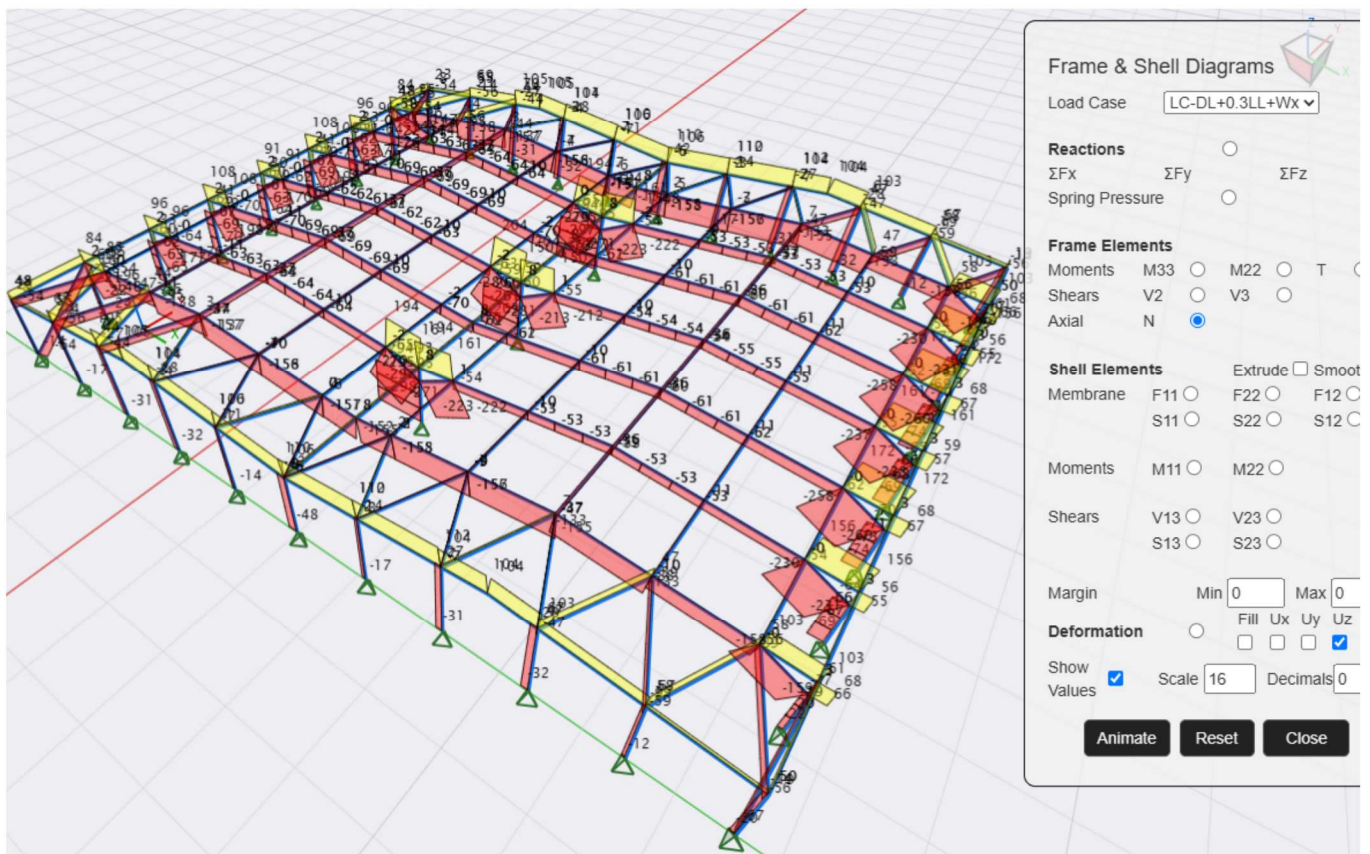
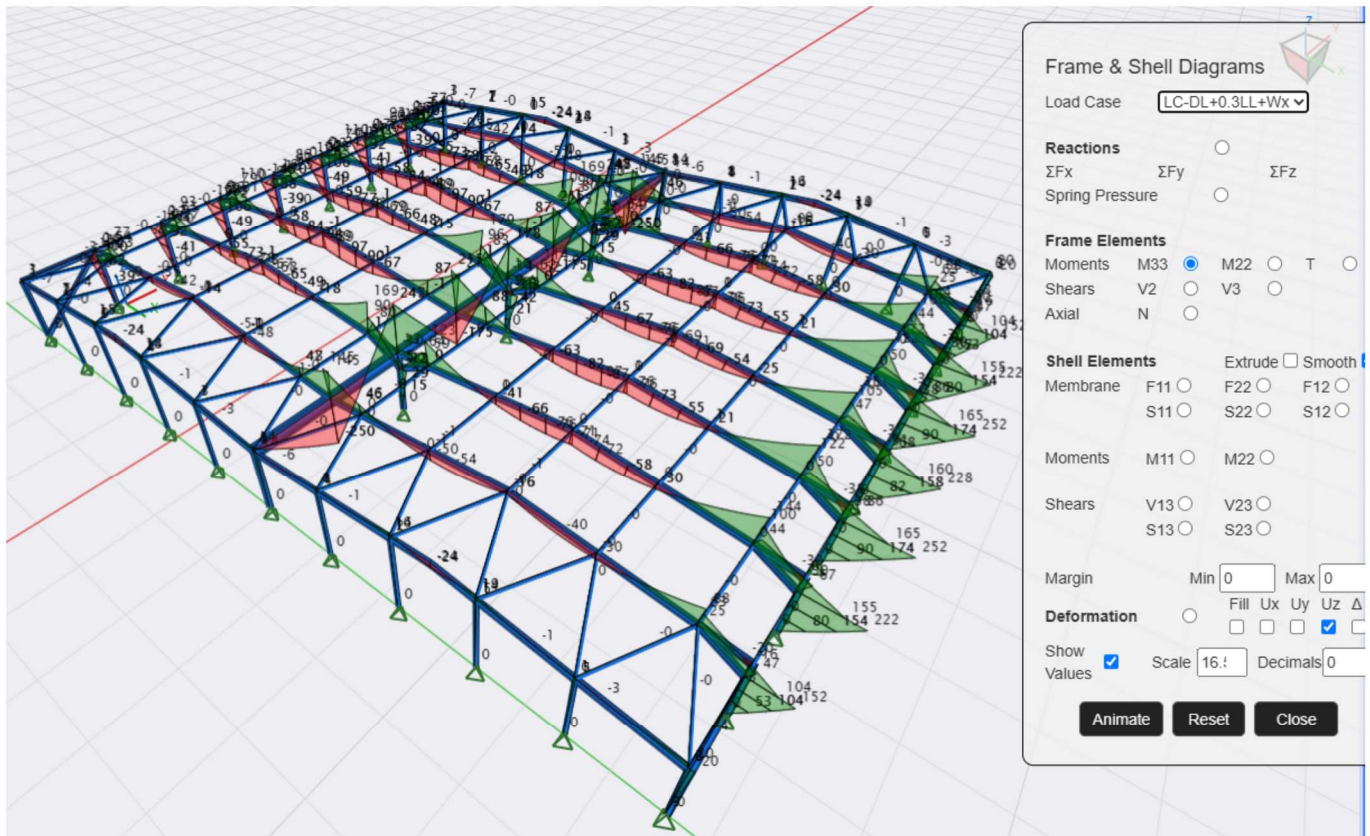
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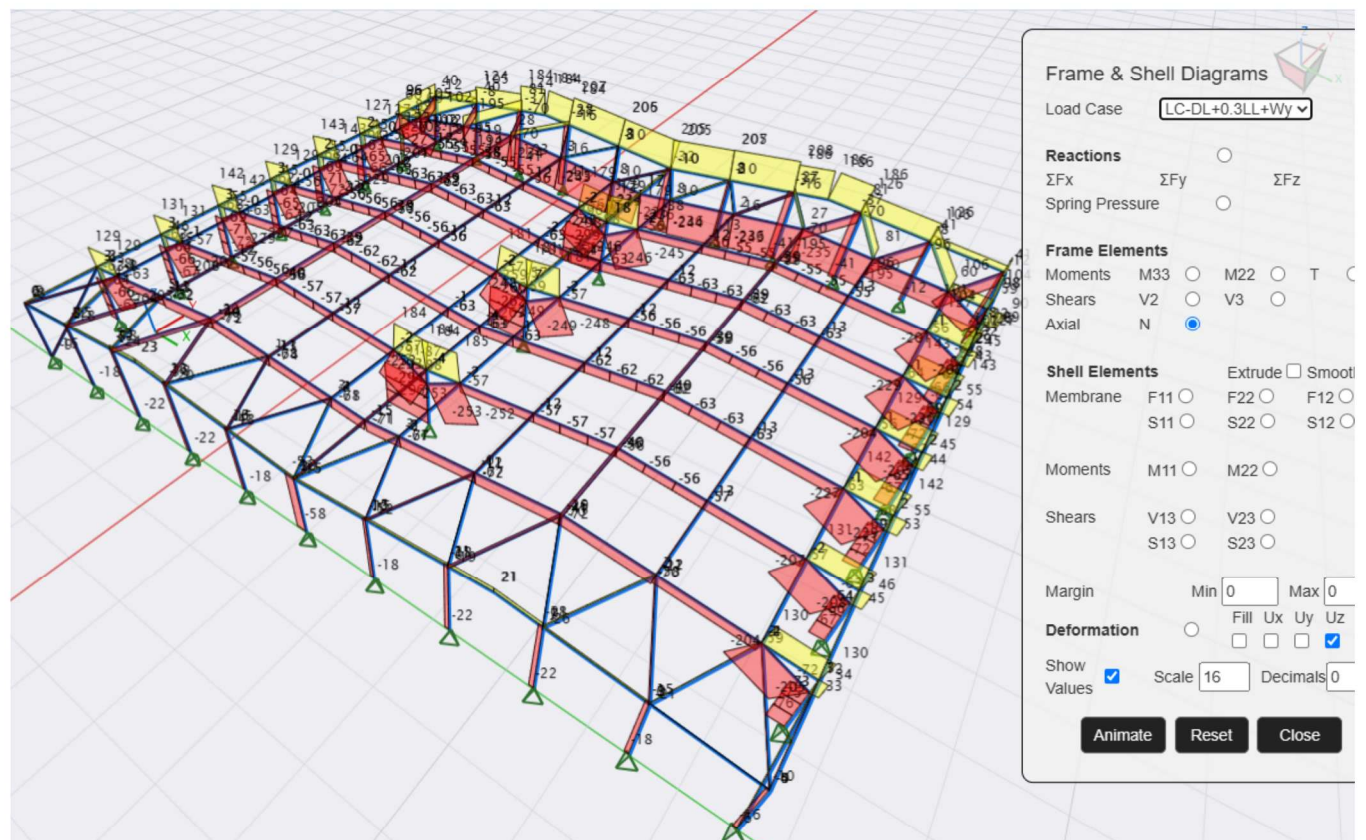
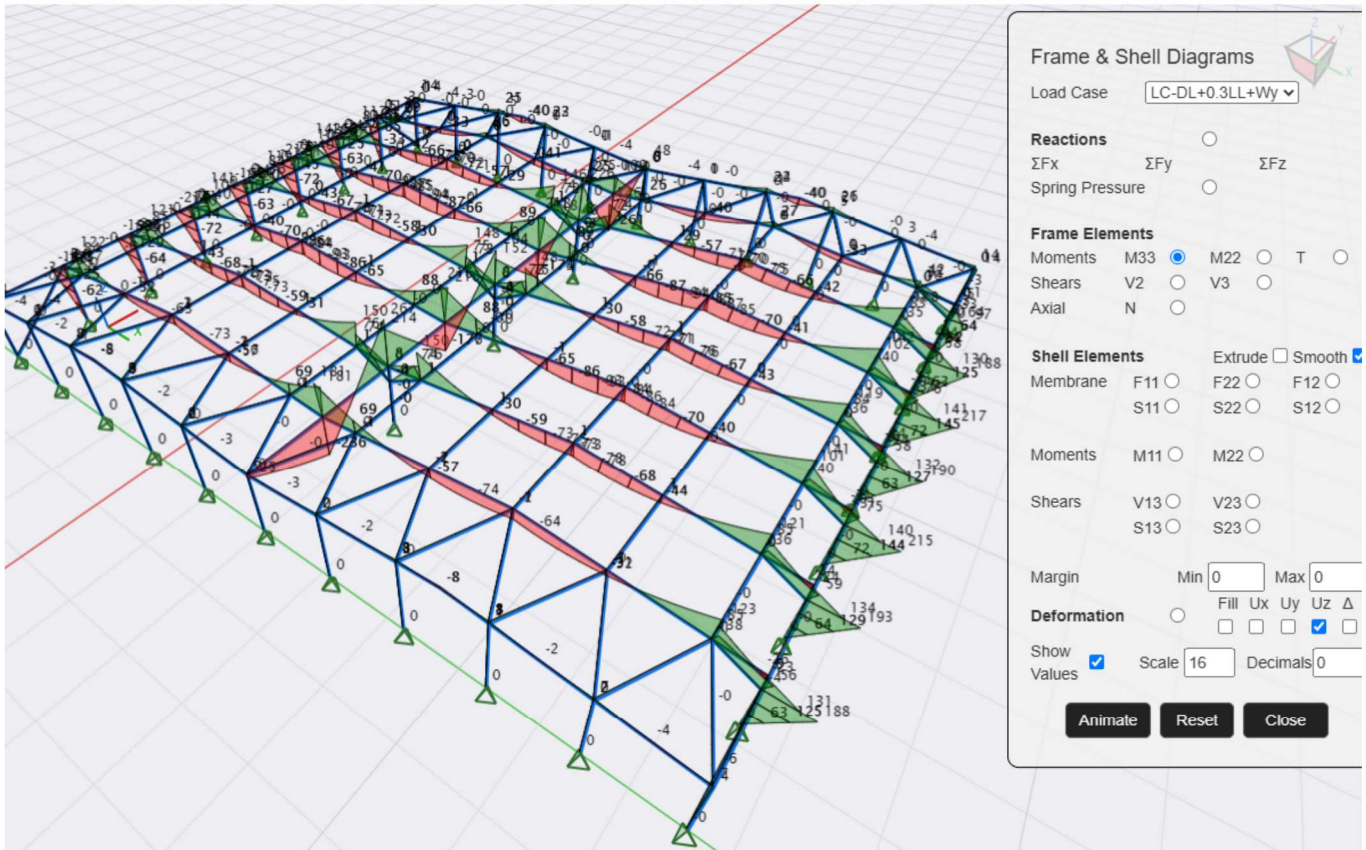
Deformation

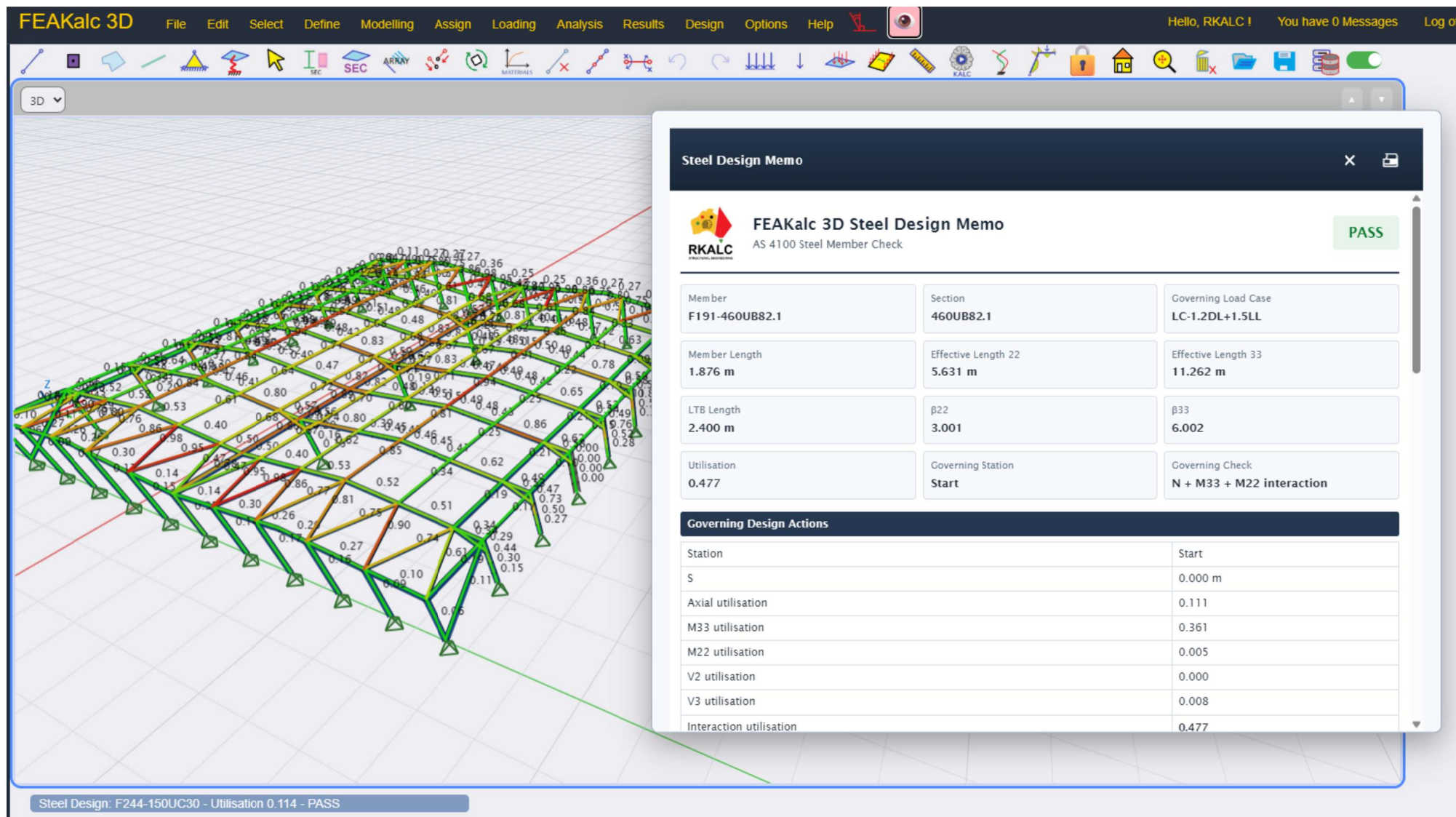
Fill Ux ☐ Uy ☐ Uz ☒

Show Values ☒ Scale: Decimals:

Animate **Reset** **Close**









Member Capacities

Navigate to steel calculator to compare rafter loads vs capacities (all pass)

I Sections

Your Design Package is valid until 30/03/2030 10:44:38 PM

Geometry

Steel Grade
Section Family
Section
Length - Axis X (mm)
Length - Axis Y (mm)



Axis X

Key Values

cs	0.89	am	1	Moa	1646
λ	11.254	ξ	32.476	αa	-2.353
cc	1	Kf	0.91	η	0
λn	11.254	ab	0	Mb/Ms	89 %

Axis Y

Key Values

cs	1.014	am	1	Moa	1646
λ	50.849	ξ	2.257	αa	20.332
cc	0.856	Kf	0.91	η	0.122
λn	50.849	ab	0	Mb/Ms	100 %

Key Properties

fy (N/mm ²)	300	fu (N/mm ²)	440
Class (X)	Compact	Class (Y)	Compact
Ze (X)	1480000	Ze (Y)	228947

Capacities

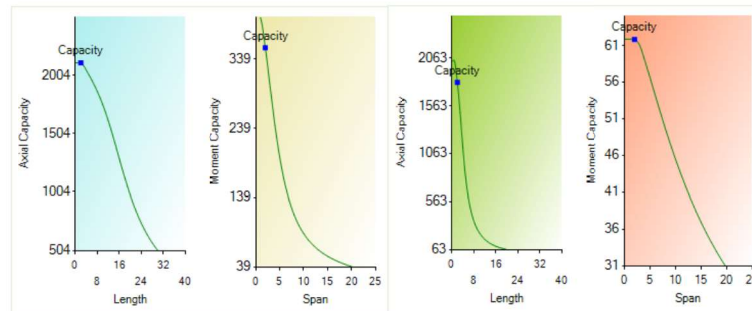
ΦM _{sx} (KN.m)	400	ΦN _{sx} (KN)	2109
ΦM _{bx} (KN.m)	356	ΦN _{cx} (KN)	2109
ΦV _{web} (KN)	667		

Capacities

ΦM _{sy} (KN.m)	62	ΦN _{sy} (KN)	2109
ΦM _{by} (KN.m)	62	ΦN _{cy} (KN)	1806

Section Properties

Depth	454	Width	190
tw	8.5	tf	12.7
Weight (kg/m)	67.35	Area	8580
I _x	2.96E+08	I _y	1.45E+07
Z _x	1303965	Z _y	152631.6
S _x	1480000	S _y	238000
r _x	185.7386	r _y	41.10933
I _w	7.06E+11	J	378000



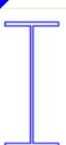
Rafters
Type 1

I Sections

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Geometry

Steel Grade
Section Family
Section
Length - Axis X (mm)
Length - Axis Y (mm)



Axis X

Key Values

cs	0.897	am	1	Moa	2161
λ	11.45	ξ	31.39	αa	-2.146
cc	1	Kf	0.968	η	0
λn	11.45	ab	0	Mb/Ms	90 %

Axis Y

Key Values

cs	1.015	am	1	Moa	2161
λ	51.208	ξ	2.234	αa	20.363
cc	0.855	Kf	0.968	η	0.123
λn	51.208	ab	0	Mb/Ms	100 %

Key Properties

fy (N/mm ²)	300	fu (N/mm ²)	440
Class (X)	Compact	Class (Y)	Compact
Ze (X)	1840000	Ze (Y)	292147

Capacities

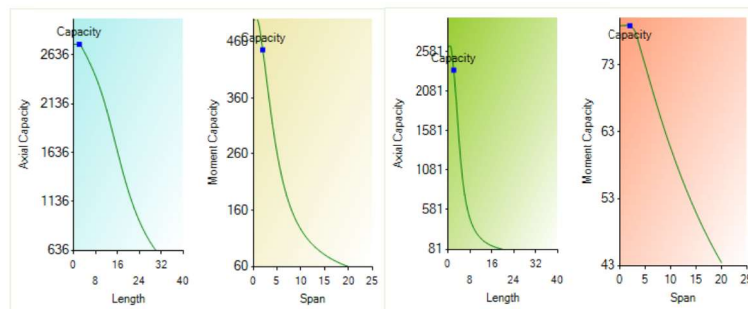
ΦM _{sx} (KN.m)	497	ΦN _{sx} (KN)	2744
ΦM _{bx} (KN.m)	446	ΦN _{cx} (KN)	2744
ΦV _{web} (KN)	787		

Capacities

ΦM _{sy} (KN.m)	79	ΦN _{sy} (KN)	2744
ΦM _{by} (KN.m)	79	ΦN _{cy} (KN)	2345

Section Properties

Depth	460	Width	191
tw	9.9	tf	16
Weight (kg/m)	82.43	Area	10500
I _x	3.72E+08	I _y	1.86E+07
Z _x	1617391	Z _y	194764.4
S _x	1840000	S _y	303000
r _x	188.2248	r _y	42.08834
I _w	9.17E+11	J	701000



Rafters
Type 2



purlins

Rafter

fly braces to
limit LTB
length

roofing
(sheeting and
insulation)

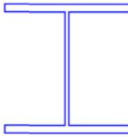


I Sections

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Geometry

Steel Grade	300
Section Family	UC
Section	310UC118
Length - Axis X (mm)	5000
Length - Axis Y (mm)	5000



Key Properties

f_y (N/mm ²)	280	f_u (N/mm ²)	440
Class (X)	Compact	Class (Y)	Compact
Z_e (X)	1960000	Z_e (Y)	881433

Section Properties

Depth	315	Width	307
tw	11.9	tf	18.7
Weight (kg/m)	117.75	Area	15000
I_x	2.77E+08	I_y	9.02E+07
Z_x	1758730	Z_y	587622.1
S_x	1960000	S_y	893000
r_x	135.8921	r_y	77.54568
I_w	1.98E+12	J	1630000

Axis X

Key Values

α_s	0.834	α_m	1	M_{oa}	1429
λ	38.939	ξ	3.393	α_a	17.984
α_c	0.909	K_f	1	η	0.083
λ_n	38.939	α_b	0	M_b/M_s	83 %

Capacities

ΦM_{sx} (KN.m)	494
ΦM_{bx} (KN.m)	412
ΦV_{web} (KN)	607

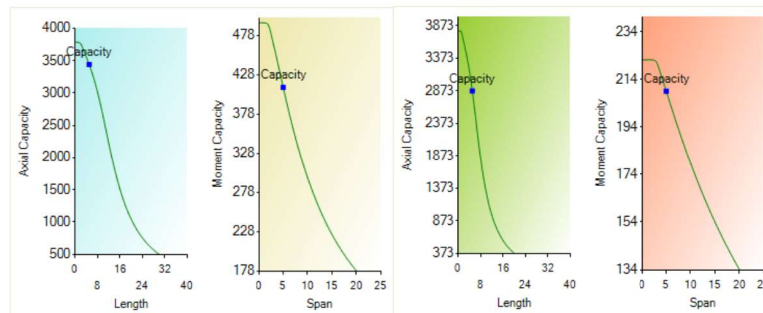
Axis Y

Key Values

α_s	0.941	α_m	1	M_{oa}	1429
λ	68.237	ξ	1.525	α_a	20.301
α_c	0.759	K_f	1	η	0.178
λ_n	68.237	α_b	0	M_b/M_s	94 %

Capacities

ΦM_{sy} (KN.m)	222	ΦN_{sy} (KN)	3780
ΦM_{by} (KN.m)	209	ΦN_{cy} (KN)	2871



Columns

