



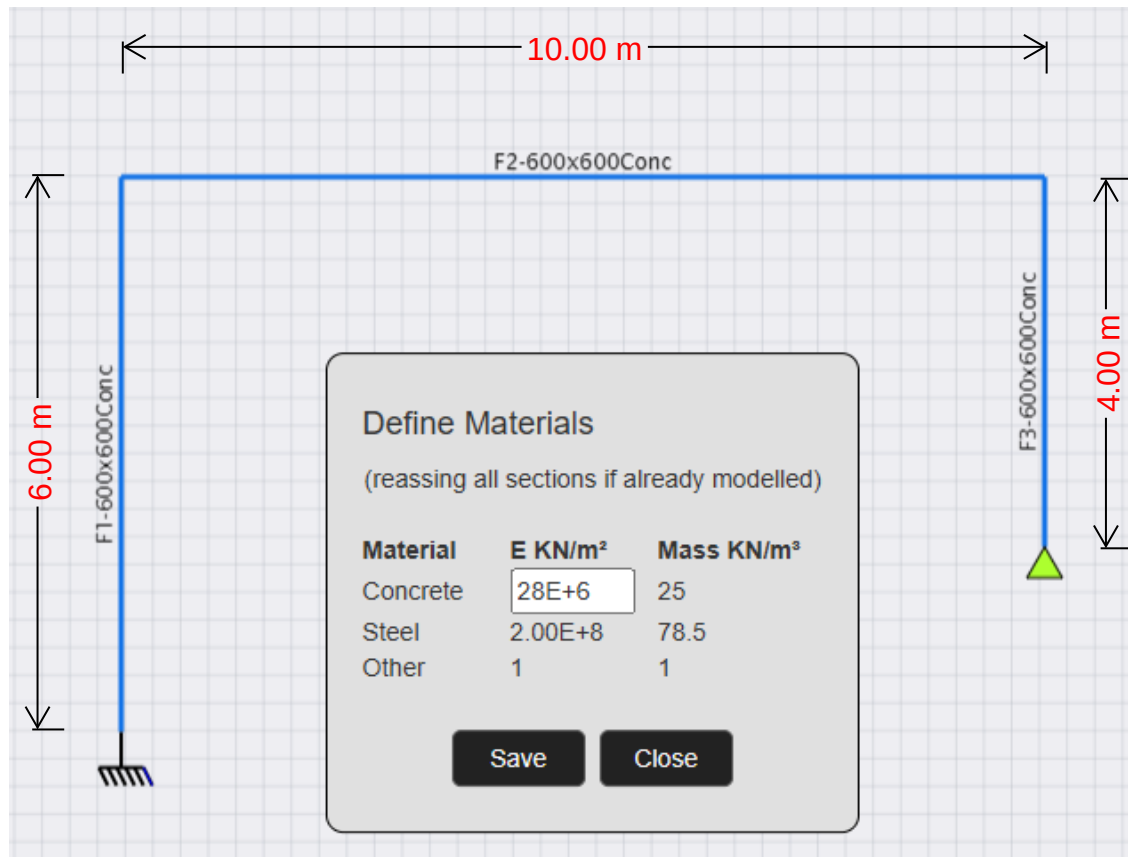
Verification example - FEAKalc 3D vs. ETABS

The frame was analysed in both FEAKalc 3D and ETABS using identical geometry, loading, member properties and support conditions. All members are 600 × 600 mm concrete sections, with $f_c = 40$ MPa and $E = 28,000$ MPa.

The comparison shows very close agreement between the two programs:

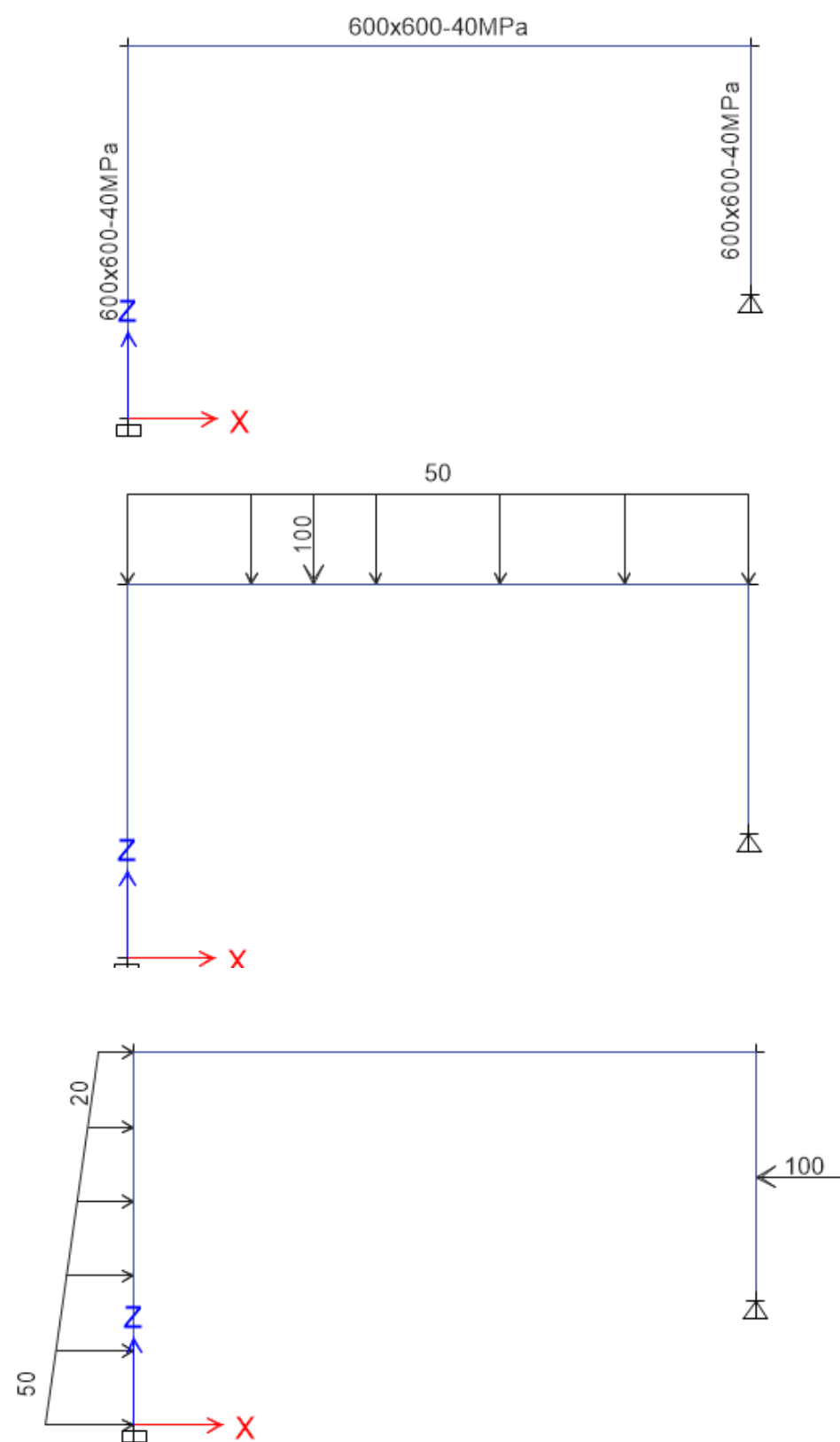
- 1- Bending moments, shear forces and axial forces are essentially identical throughout the frame.
- 2- The maximum beam sagging moment is 490.36 kNm in FEAKalc 3D, compared with 490.73 kNm in ETABS (agreement within 0.075 %)
- 3- The principal joint and column forces generally match to the displayed precision.
- 4- At the upper-right joint, both programs calculate a horizontal displacement of 1.682 mm and a vertical displacement of -0.165 mm (identical)

Overall, the example demonstrates excellent correlation between FEAKalc 3D and ETABS for frame actions and nodal displacements.

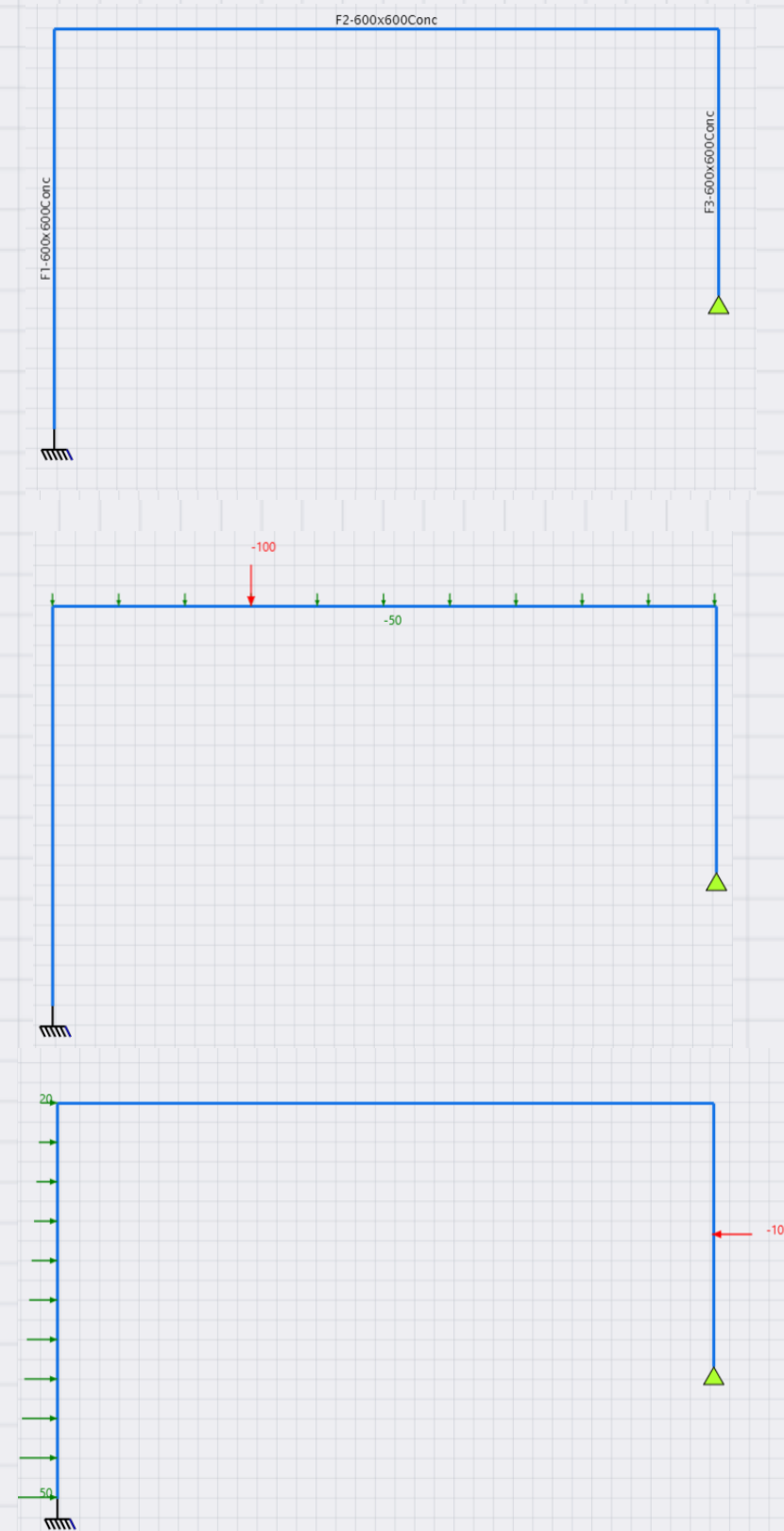




ETABS

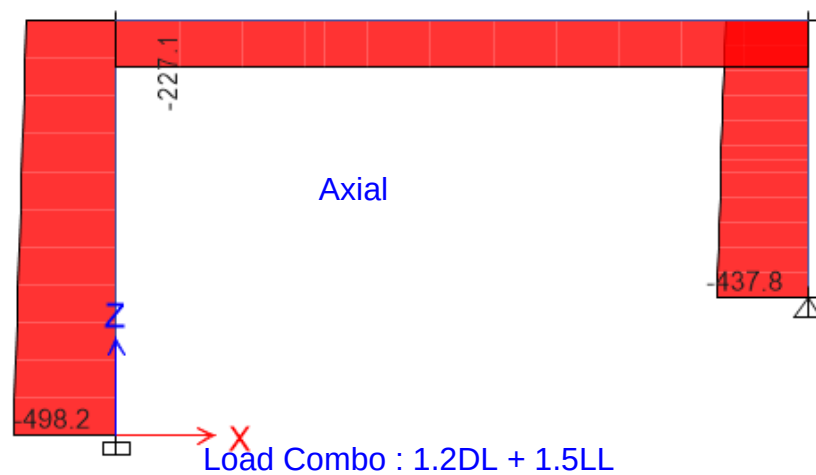
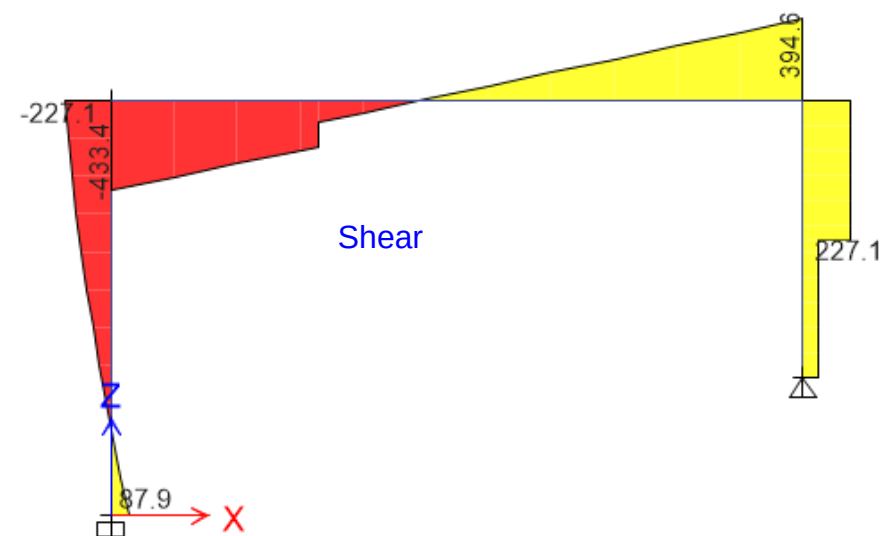
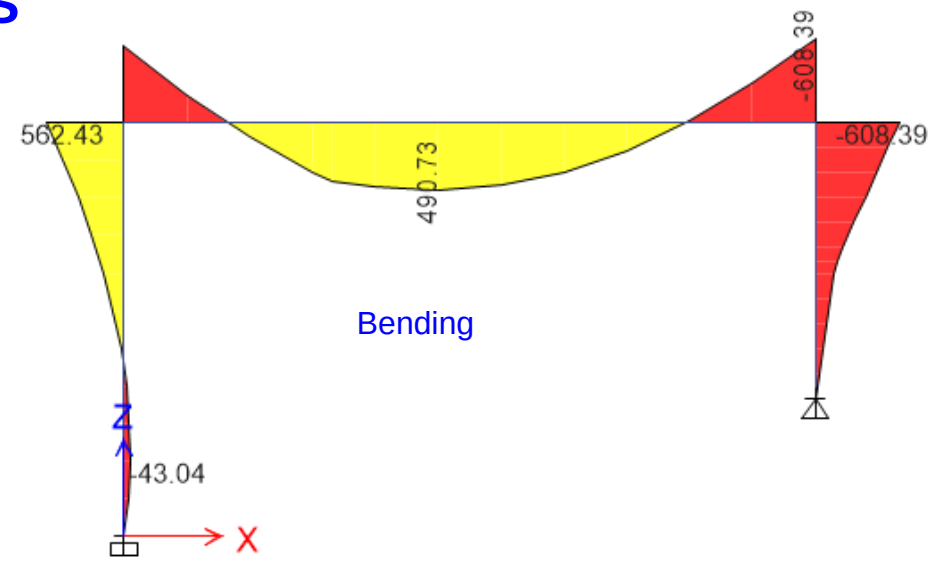


FEAKalc 3D

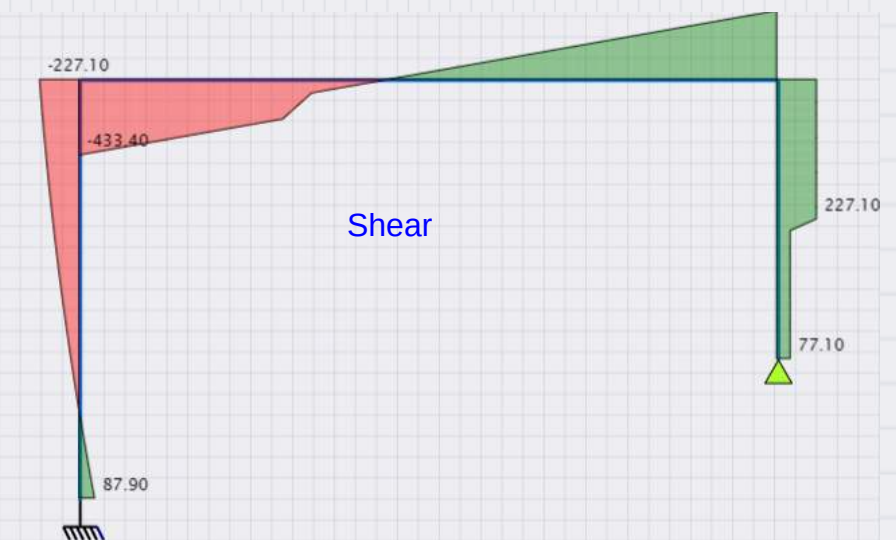
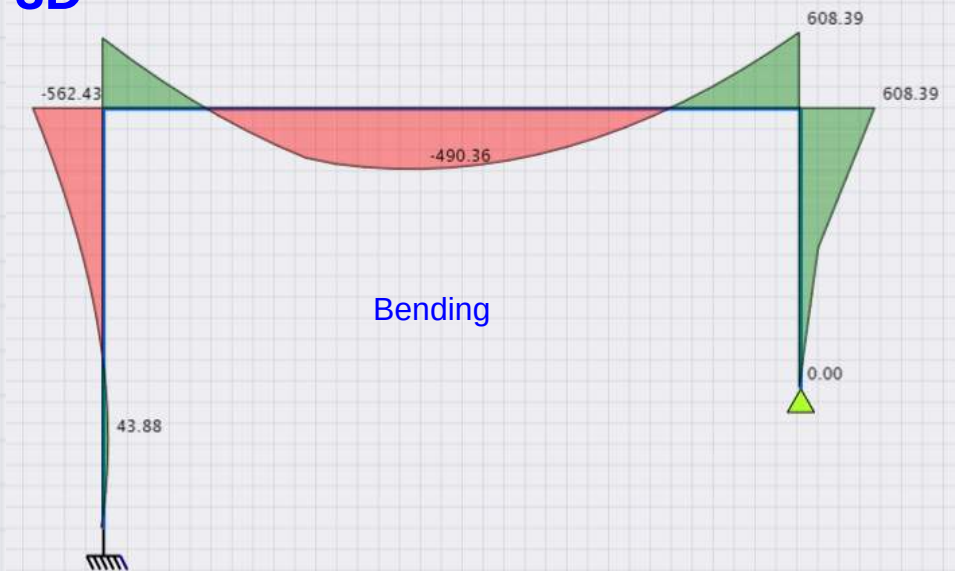




ETABS



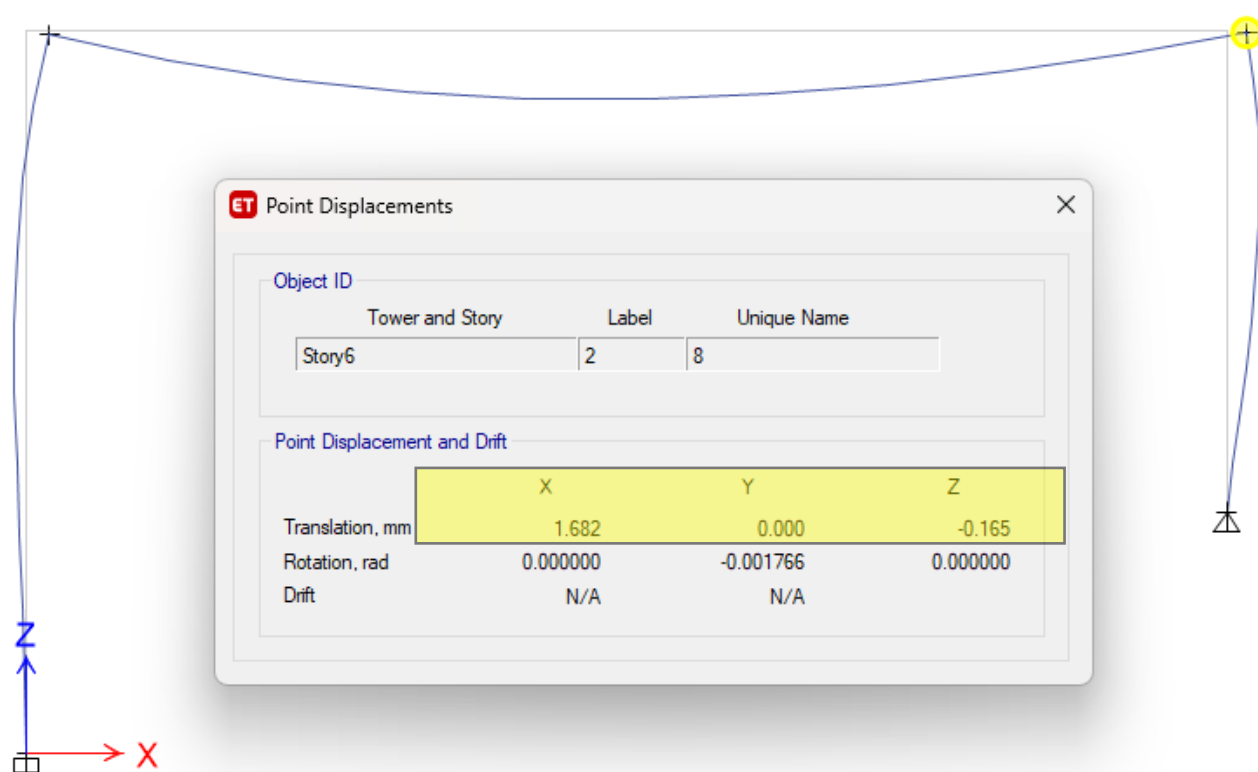
FEAKalc 3D





ETABS

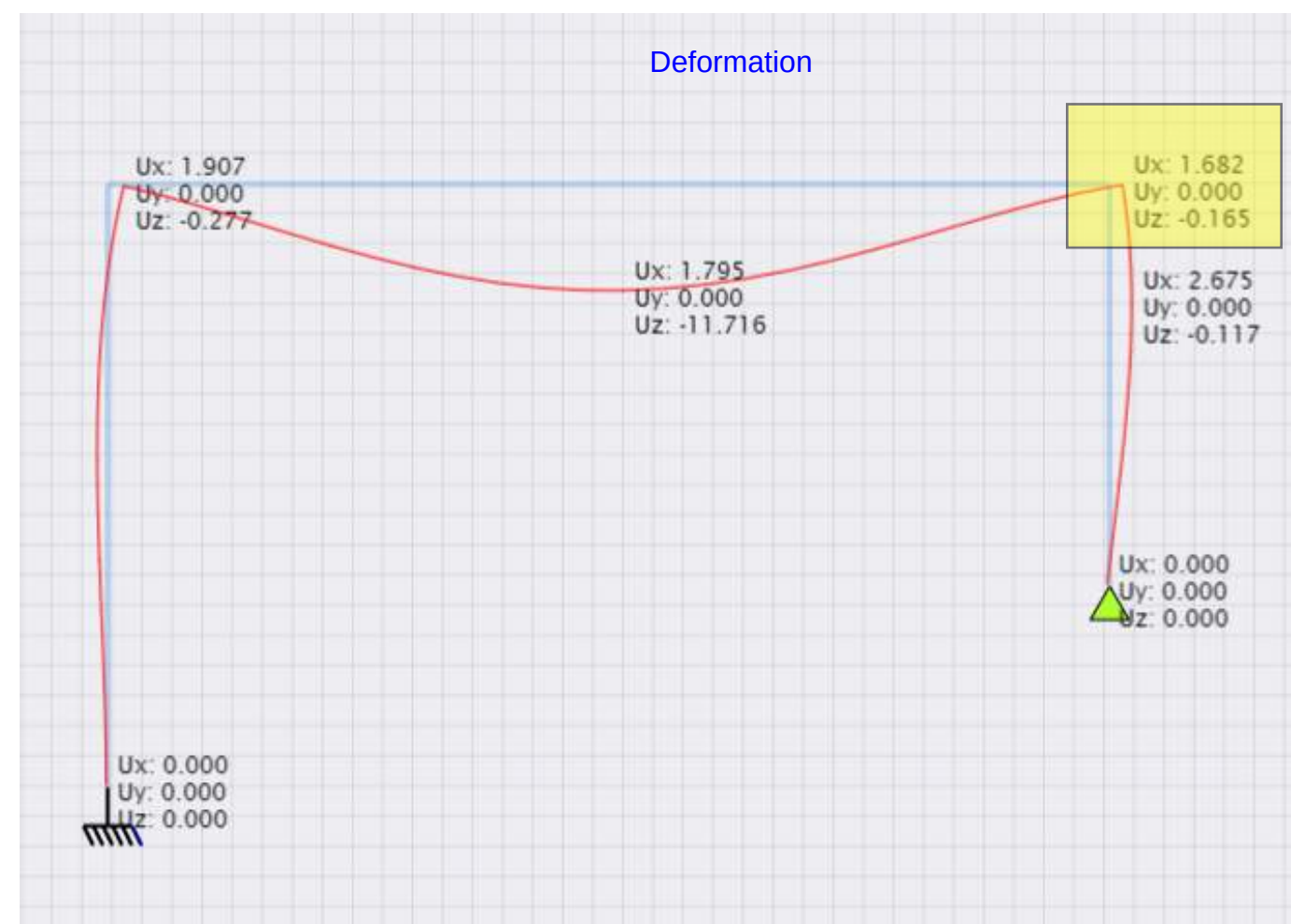
Deformation



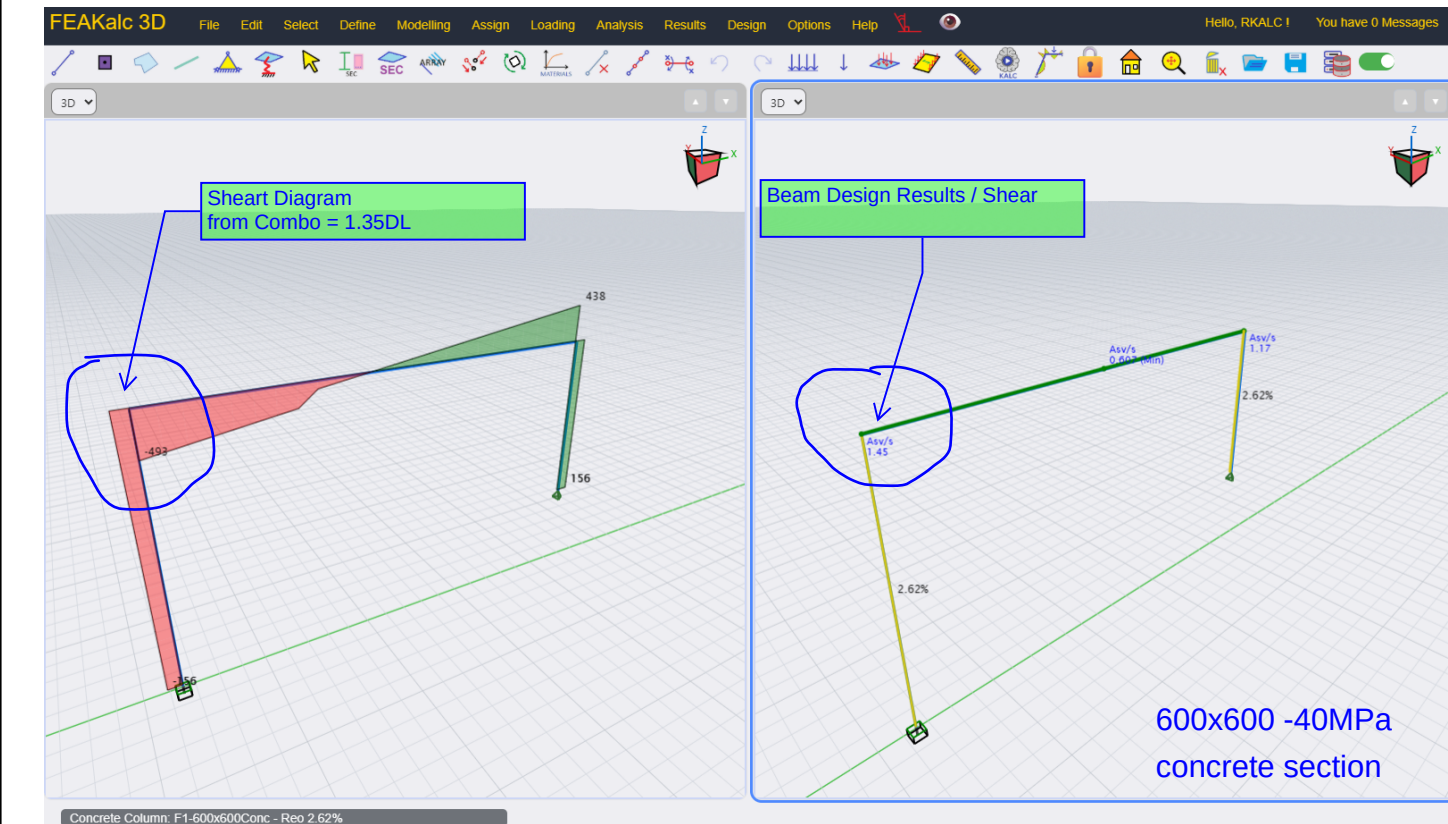
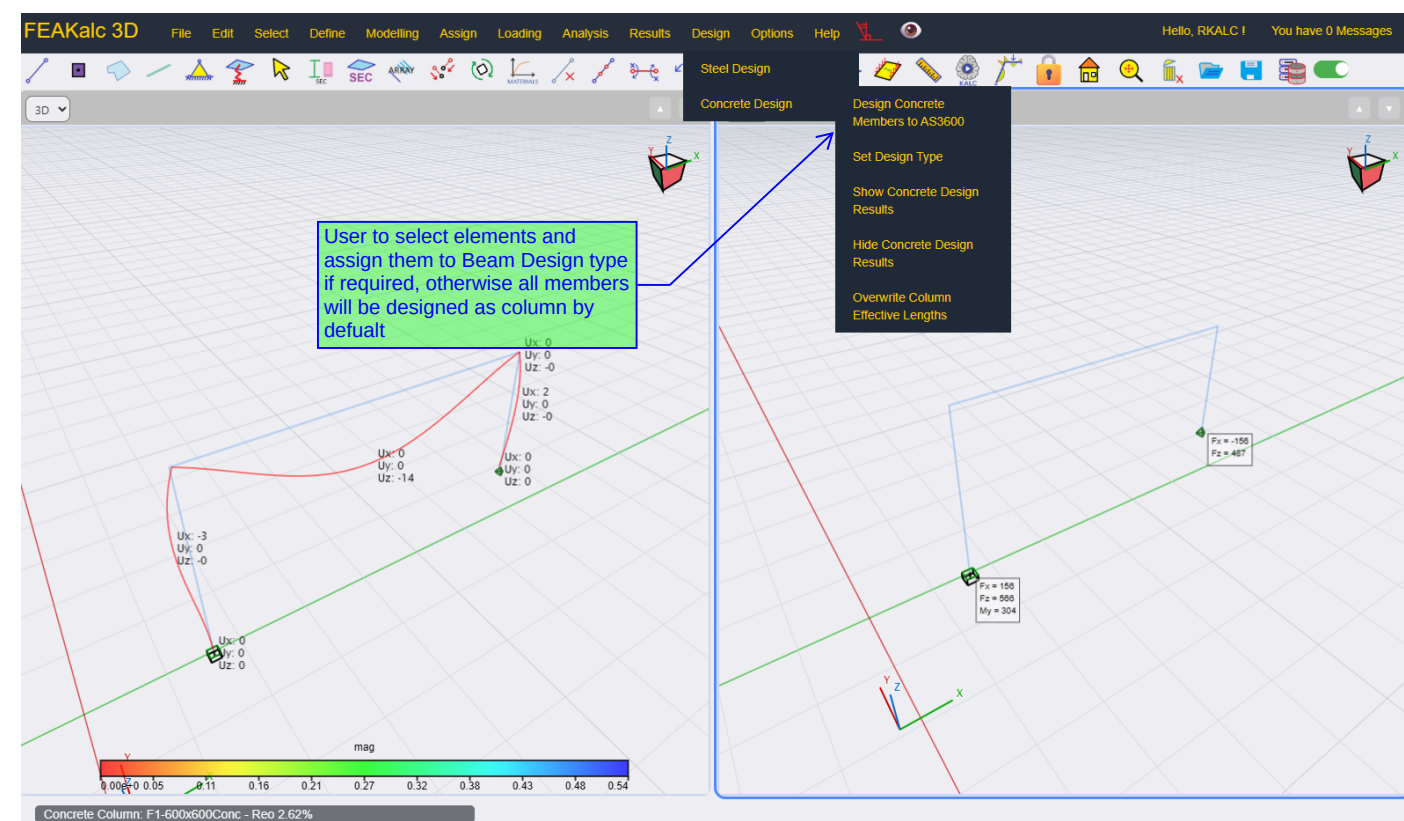
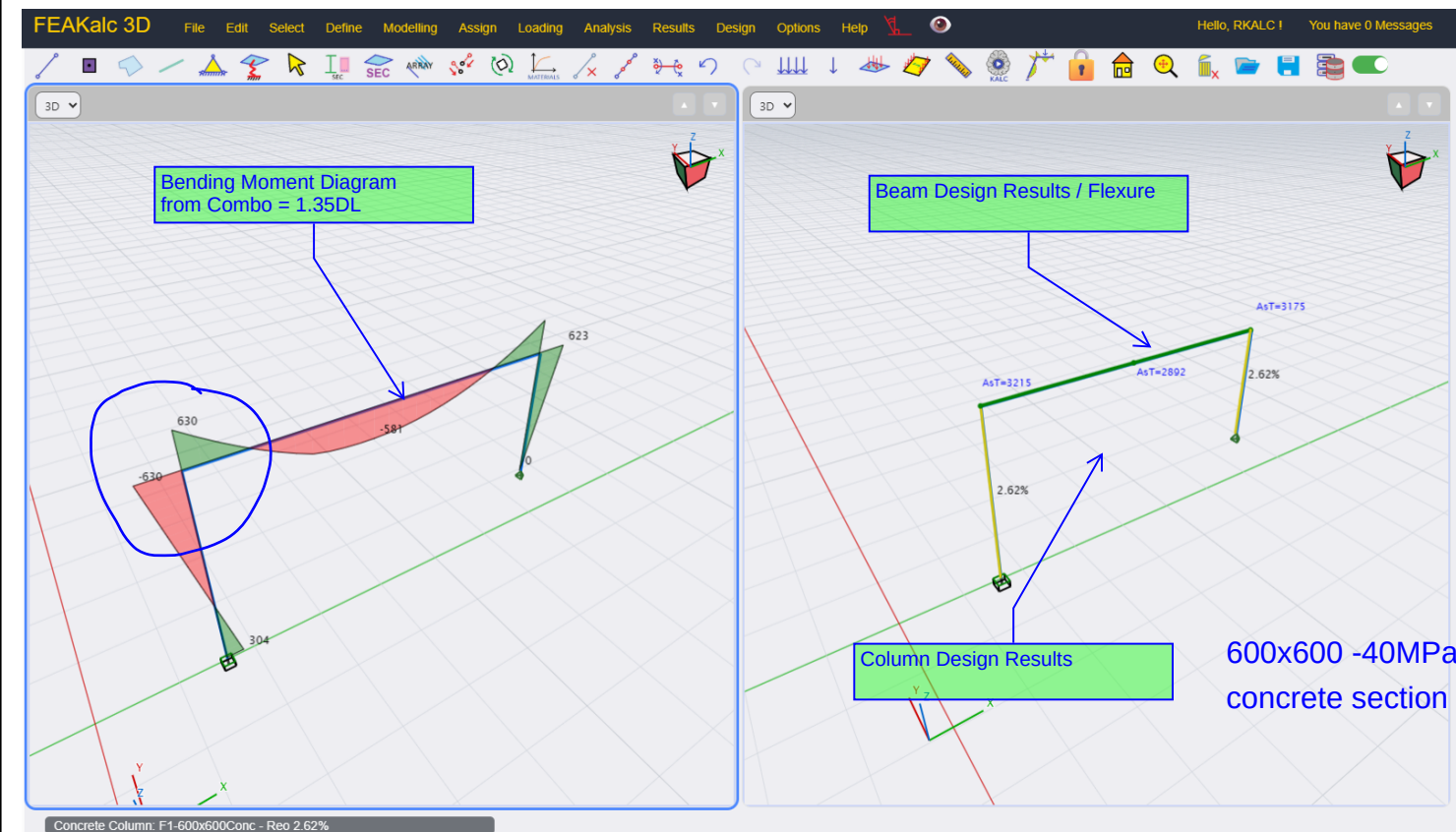
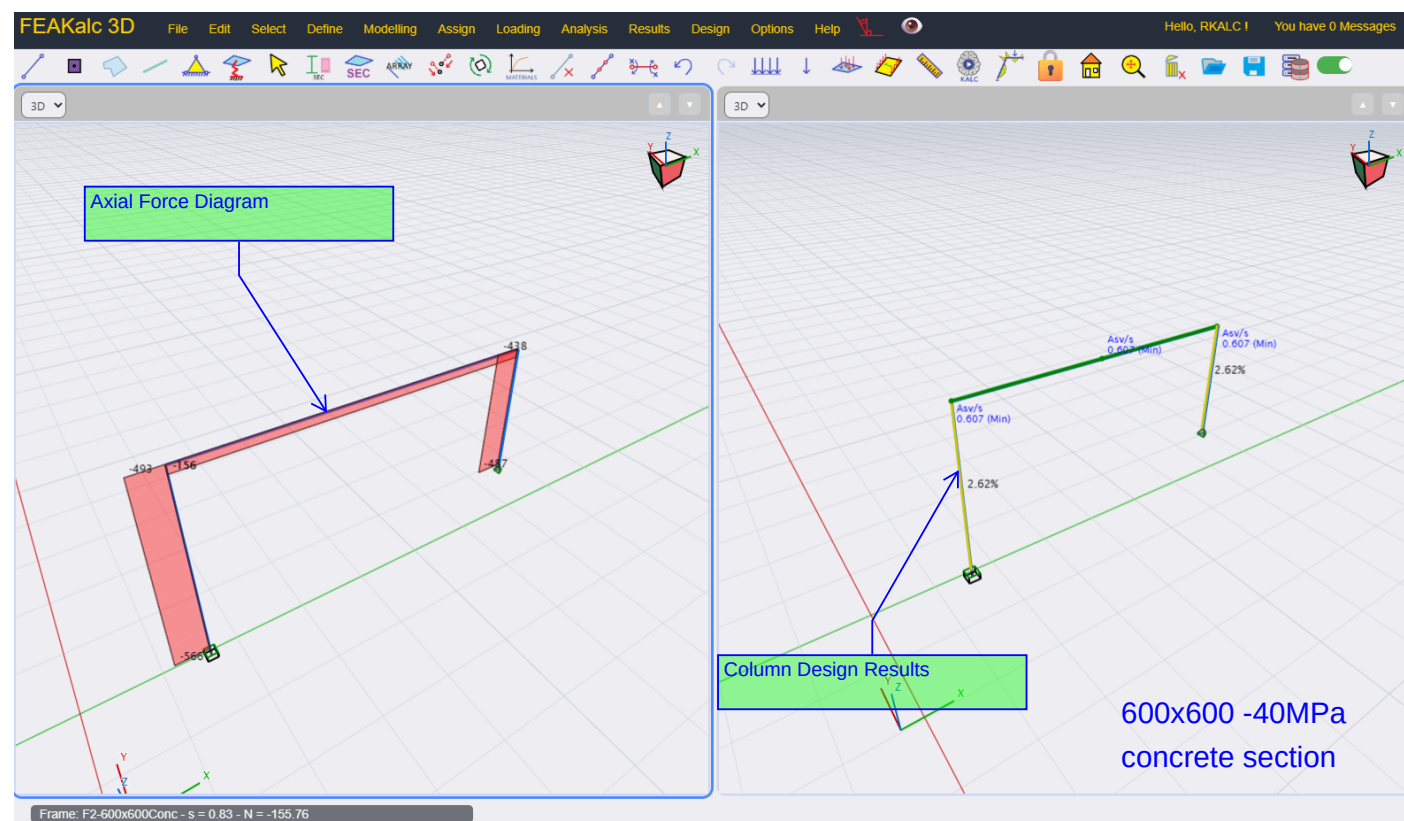
Load Combo : 1.2DL + 1.5LL

FEAKalc 3D

Deformation



Load Combo : 1.2DL + 1.5LL





Column Design Report



FEAKalc 3D Concrete Column Design Memo

AS 3600 RC Column Check

PASS

Member F1	Governing Load Case LC-1.35DL	Governing Section 600 x 600
f' _c 40 MPa	f _y 500 MPa	Cover to Reo Centre 54 mm
Effective Length 22 6000 mm	Effective Length 33 6000 mm	Design Height 6000 mm
Bars 7 x 10 N20	Reinforcement 2.62 %	Utilisation 85 %

Applied Design Actions

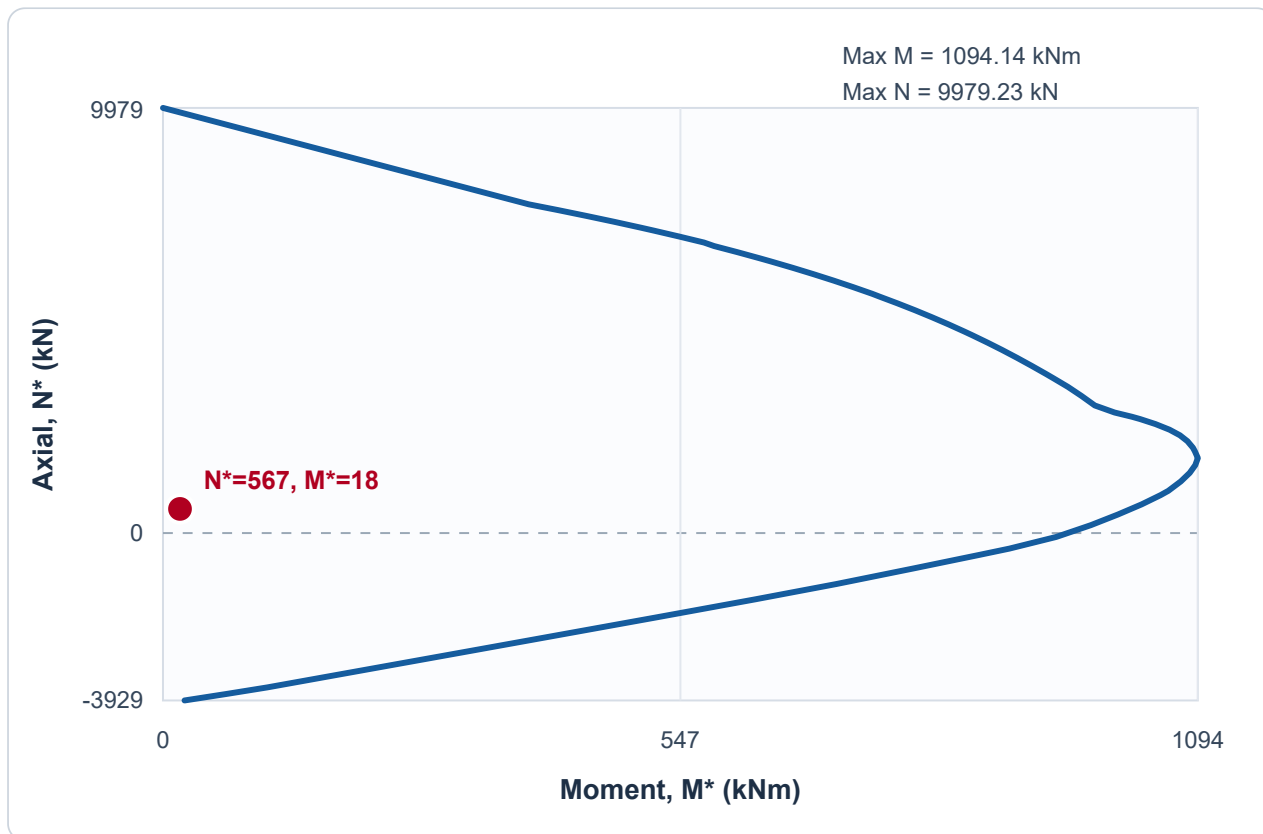
Item	Value
N*	567 kN
M22 top	16.99 kNm
M22 bottom	-16.99 kNm
M33 top	630.36 kNm
M33 bottom	-630.36 kNm

Direction 22 Column Check

Item	Value
Balanced moment capacity	995 kNm
Euler buckling force, N _{cr}	14689 kN
K _m	1.00
Moment magnifier, δ _b	1.04
Pure bending capacity	963.00 kNm
Design moment, M22*	18.00 kNm
N / b _d index	1.58
M / b _d ² index	0.08
Utilisation	7.000000000000001%



Interaction Diagram - Direction 22

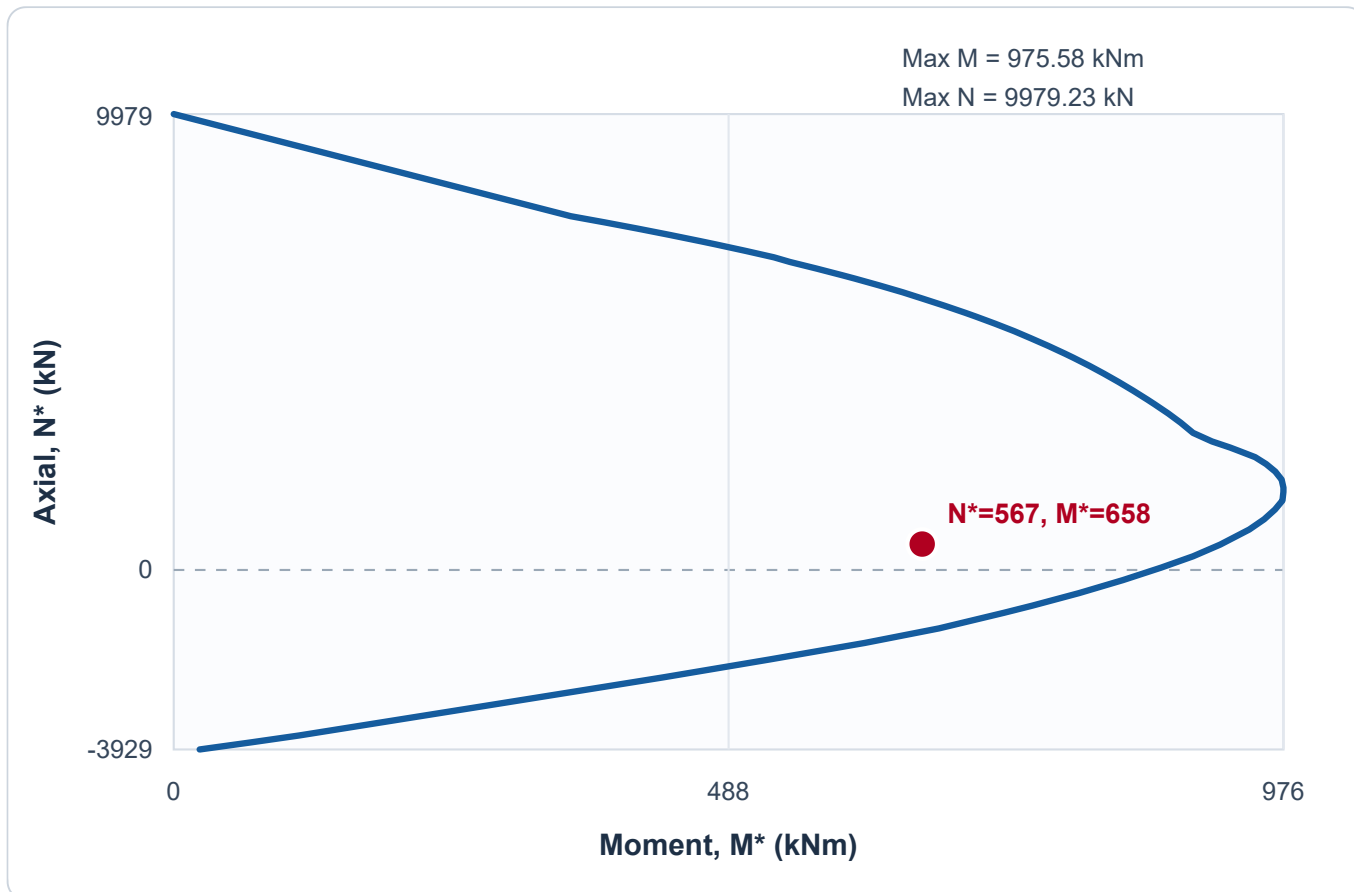


Direction 33 Column Check

Item	Value
Balanced moment capacity	904.00 kNm
Euler buckling force, Ncr	13340 kN
Km	1.00
Moment magnifier, δ_b	1.04
Pure bending capacity	868.00 kNm
Design moment, M33*	658.00 kNm
N / bd index	1.58
M / bd ² index	3.05
Utilisation	71%



Interaction Diagrams- Direction 33

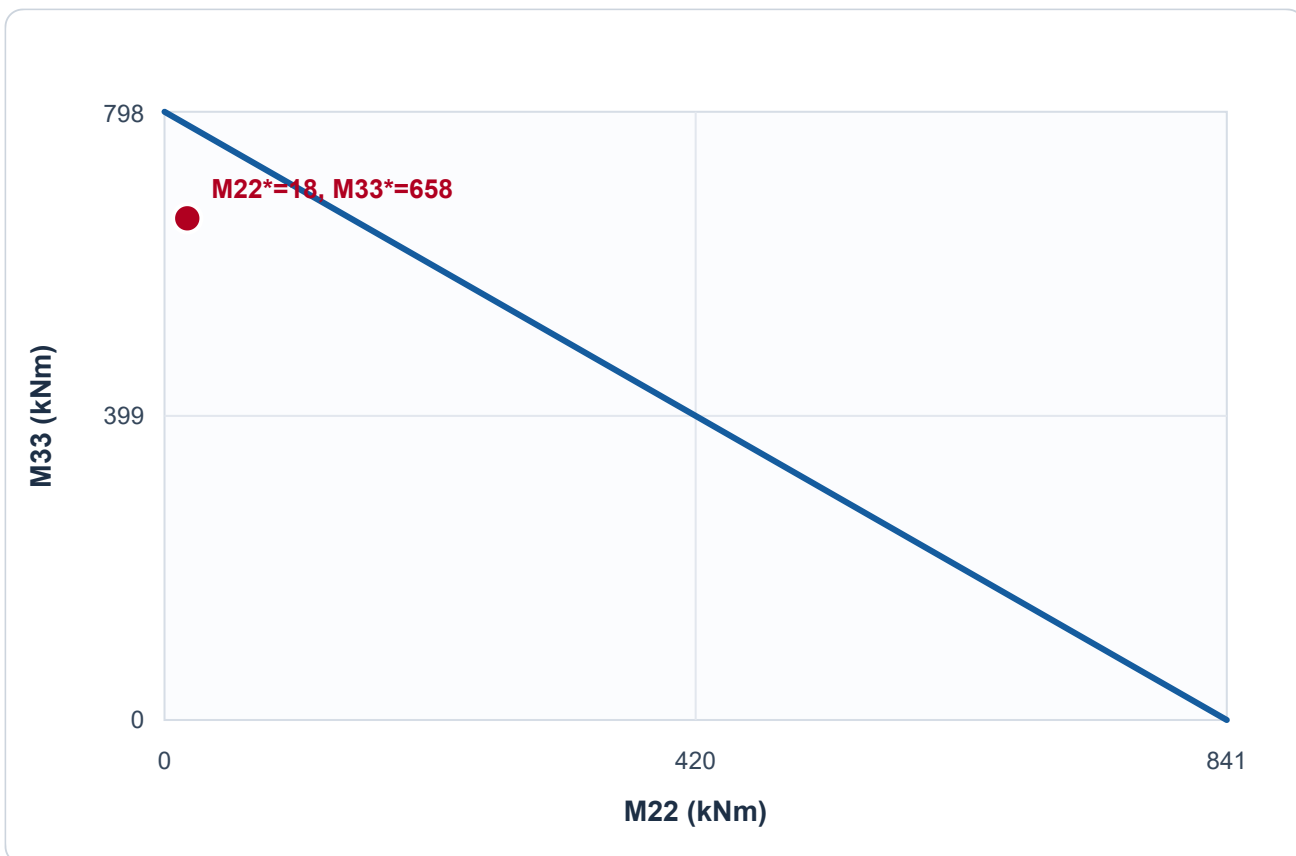


Axial and Biaxial Capacity

Item	Value
Squash load	9979 kN
Pure tension capacity	4006 kN
Muo 22	841.00 kNm
Muo 33	798.00 kNm
Biaxial power, α_b	1.00
Biaxial utilisation	85%



Biaxial Interaction Diagram



Design Notes

Column reinforcement is selected from the concrete optimisation result.
The red marker represents the governing applied design action on each principal axis.



Following is a critical point cross check at corner (eave) of the frame where
moment = 630 and co-existing shear = 493

Your Design Package is valid until 30/03/2030 10:44:38 PM

Inputs

Materials

f'_c (N/mm²)

f_y (N/mm²)

f_{ys} (N/mm²)

Flexural Rebar Dia mm

Shear Rebar Dia mm

$\alpha=0.79$ / $\gamma=0.87$

Geometry (Units mm)

Width

Depth

Bot. Cover to Centre

Top Cover to Centre

Torsion Cover (clear)

Loads (KN , m)

Moment (ULS)

Moment (SLS)

$M/bd^2=3.53$

Shear - Coexisting

Torsion - Coexisting

Axial force - for Shear
(-ve for compression)

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NA d.=89 / $K_u=0.1633$ / $\Phi=0.85$

Flexural Reo

As (mm²) - Required Bot.

As - Adopted Bot **26N12**

fs Mpa (tension Reo)

As' (mm²) - Required Top

Adopted Top

fs Mpa (comp Reo)

Φ_{Mub} (Max-Single)

Flexural Capacity

Shear & Torsion

V_{eq} (KN)

Shear Stress

Permitted Shear

$\epsilon =$

$\theta_v =$

$K_v =$

ΦT_{cr} (KN.m)

ΦV_c (N/mm²)

V_s (N/mm²)

ΔF_{td} (KN)

Cl. 8.2.7 REO

A_{sw}/S (mm²/mm)

A_{sv}/S (mm²/mm)

Min Shear Legs

Required Spacing